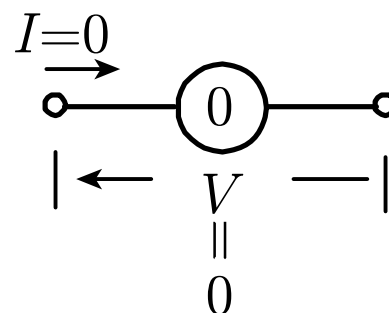
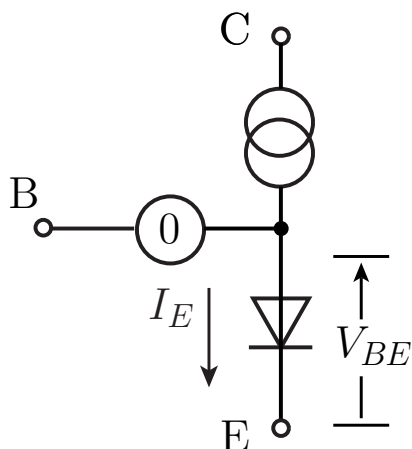


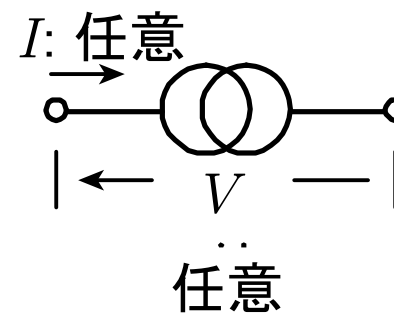
差動増幅回路の大信号特性と OTA(電圧制御電流源回路)

バイポーラ差動増幅回路の大信号特性

バイポーラトランジスタのモデル(大信号モデル)



(a) ナレータ

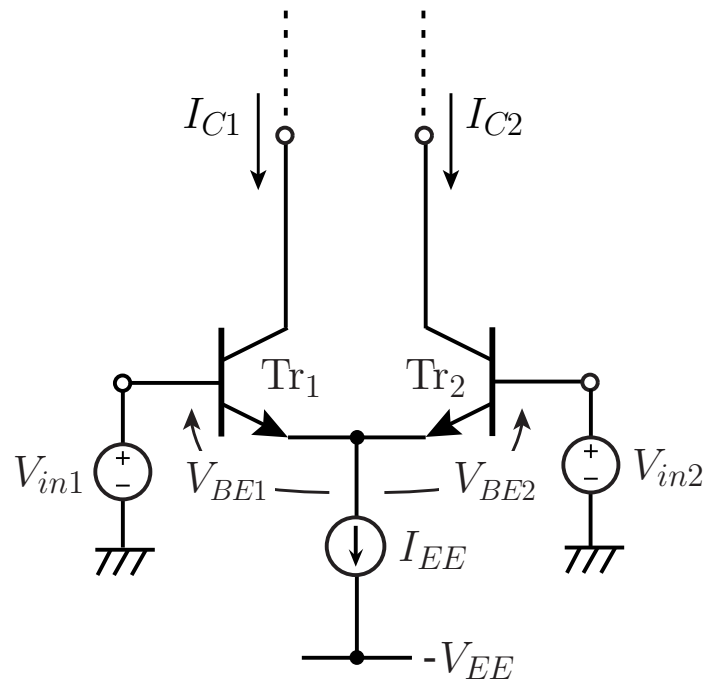


(b) ノレータ

$$I_E = I_{ES} \exp\left(\frac{qV_{BE}}{kT}\right)$$

$$I_C = I_E$$

バイポーラ差動増幅回路



$$V_{in1} - V_{BE1} + V_{BE2} - V_{in2} = 0$$

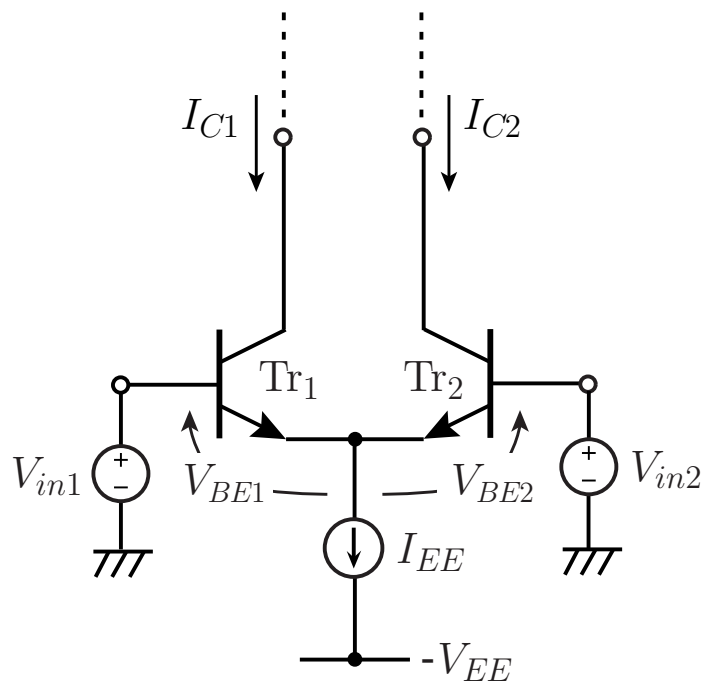
$$\Delta V_{in} = V_{in1} - V_{in2} = V_{BE1} - V_{BE2}$$

$$V_{BEi} = \frac{kT}{q} \ln\left(\frac{I_{Ei}}{I_{ES}}\right)$$

$$\Delta V_{in} = \frac{kT}{q} \ln\left(\frac{I_{E1}}{I_{ES}}\right) - \frac{kT}{q} \ln\left(\frac{I_{E2}}{I_{ES}}\right)$$

$$I_{Ci} = I_{Ei}$$

$$= \frac{kT}{q} \ln\left(\frac{I_{E1}}{I_{E2}}\right)$$



$$\frac{I_{E1}}{I_{E2}} = \exp\left(\frac{q\Delta V_{in}}{kT}\right)$$

$$I_{E1} + I_{E2} = I_{EE}$$

$$I_{E1} = \frac{I_{EE}}{1 + \exp\left(\frac{-q\Delta V_{in}}{kT}\right)}$$

$$I_{E2} = \frac{I_{EE}}{1 + \exp\left(\frac{+q\Delta V_{in}}{kT}\right)}$$

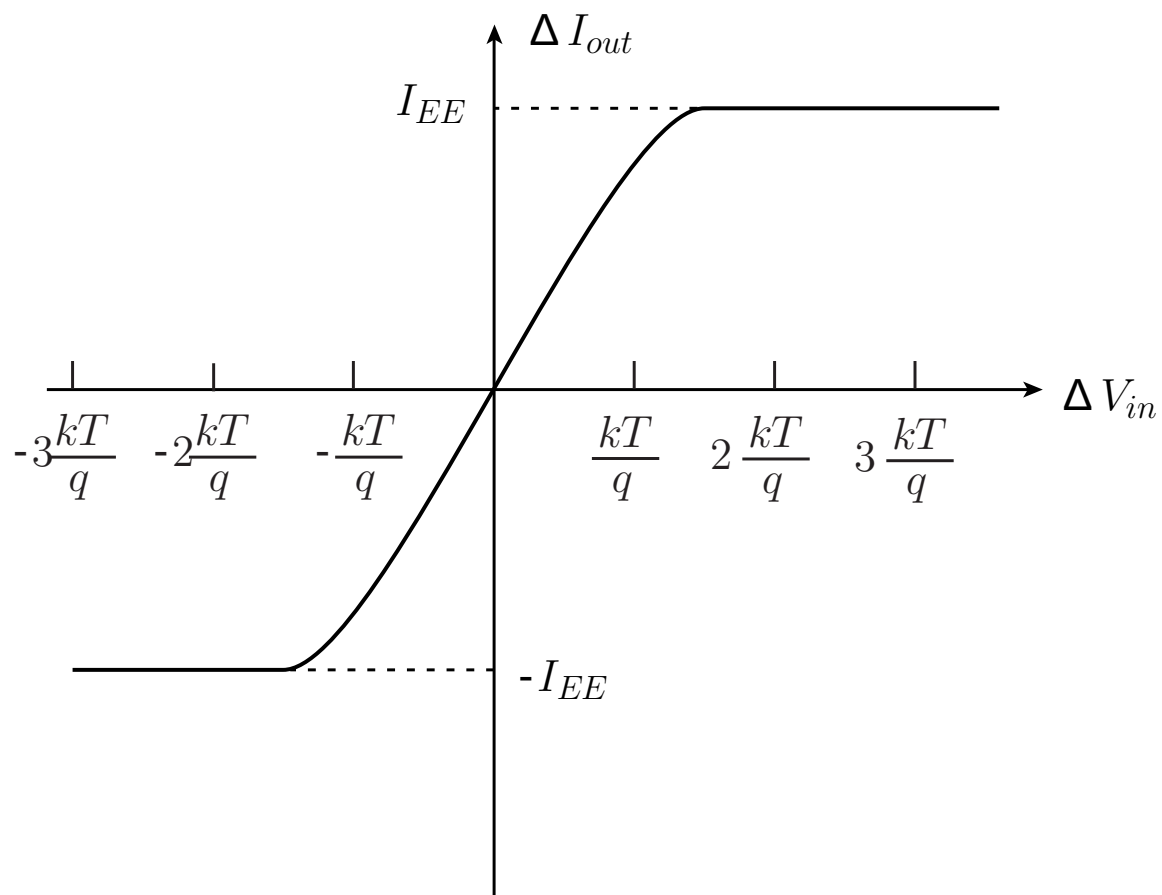
$$I_{E1} = \frac{I_{EE}}{1 + \exp\left(\frac{-q\Delta V_{in}}{kT}\right)} \quad I_{E2} = \frac{I_{EE}}{1 + \exp\left(\frac{+q\Delta V_{in}}{kT}\right)}$$

$$\Delta I_{out} = I_{C1} - I_{C2} = I_{E1} - I_{E2}$$

$$= I_{EE} \left(\frac{1 - \exp\left(\frac{-q\Delta V_{in}}{kT}\right)}{1 + \exp\left(\frac{-q\Delta V_{in}}{kT}\right)} \right)$$

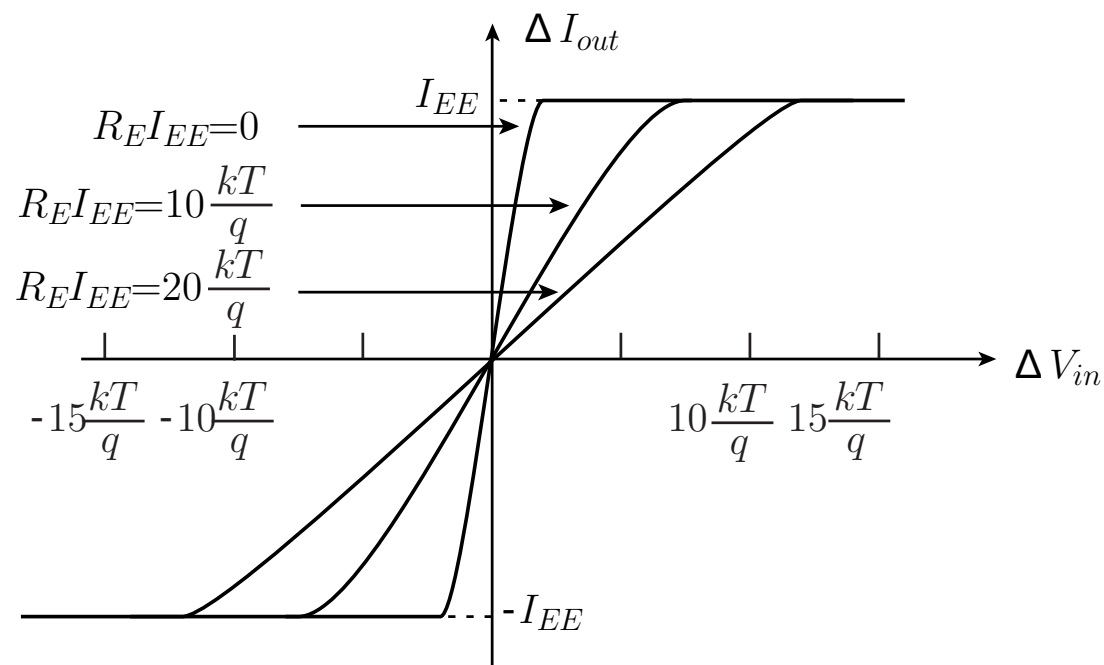
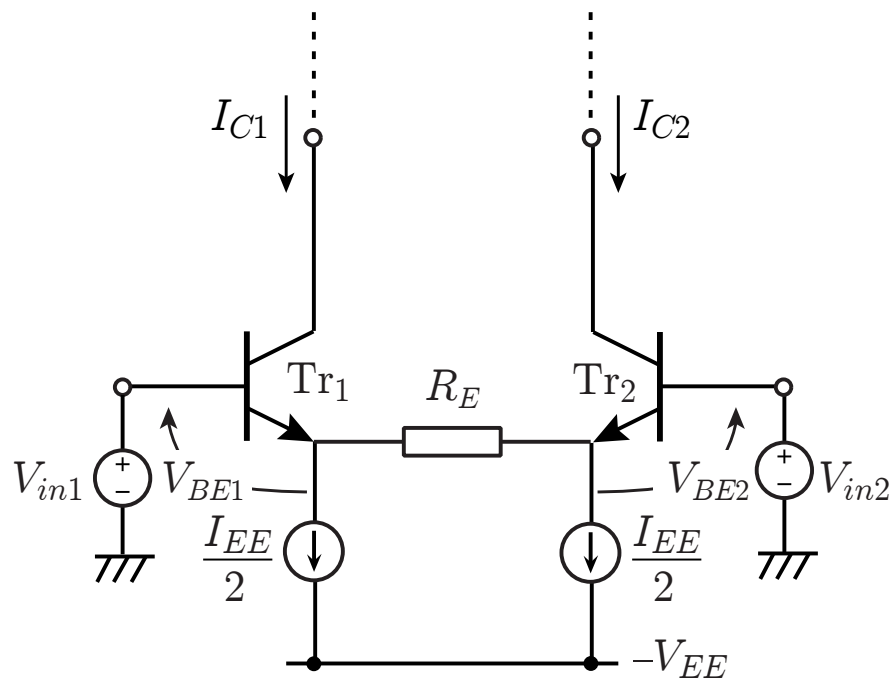
$$= I_{EE} \left(\frac{\exp\left(\frac{q\Delta V_{in}}{2kT}\right) - \exp\left(\frac{-q\Delta V_{in}}{2kT}\right)}{\exp\left(\frac{q\Delta V_{in}}{2kT}\right) + \exp\left(\frac{-q\Delta V_{in}}{2kT}\right)} \right) = I_{EE} \tanh\left(\frac{q\Delta V_{in}}{2kT}\right)$$

バイポーラ差動増幅回路の大信号特性



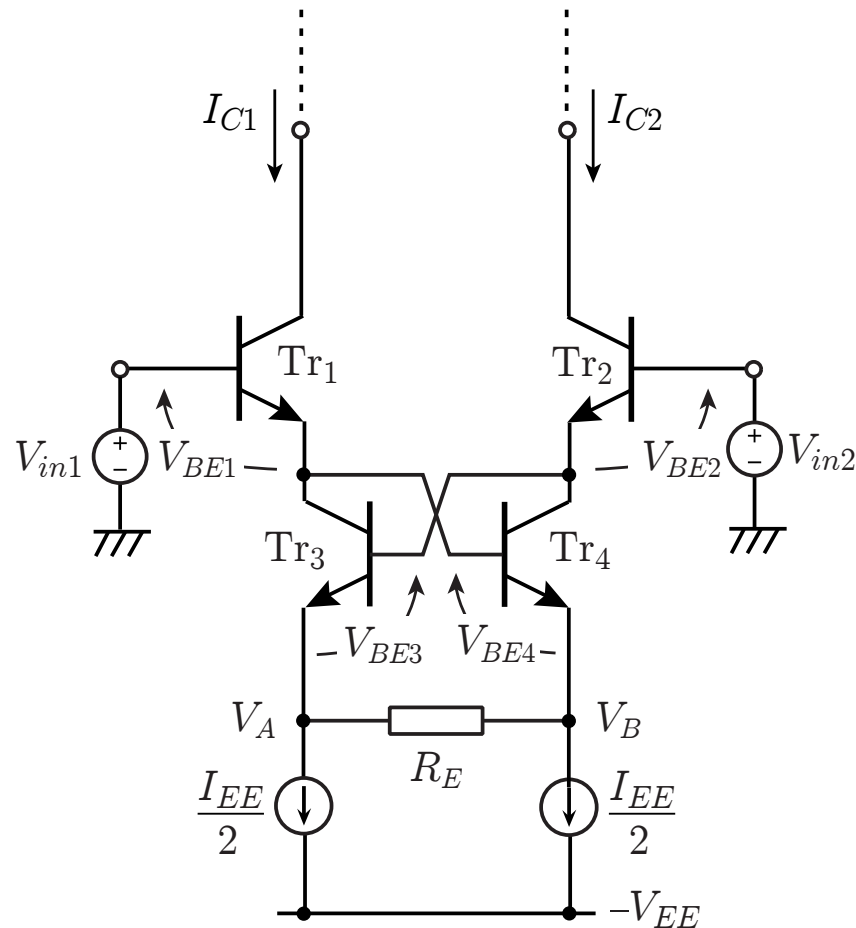
線形範囲: 数十mV程度

線形入力範囲の拡大



伝達コンダクタンスの低減

Caprio's Quad



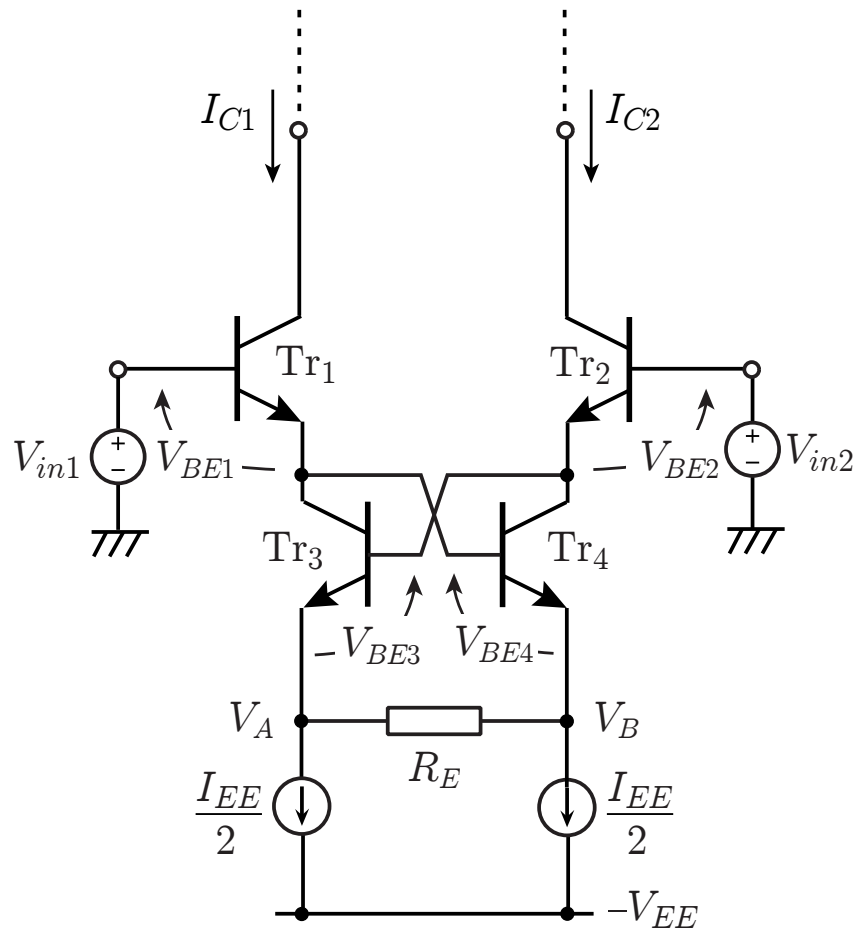
$$V_{BE} = \frac{kT}{q} \ln\left(\frac{I_E}{I_{ES}}\right)$$

$$\begin{matrix} I_{E1} = I_{E3} \\ I_{E2} = I_{E4} \end{matrix} \longrightarrow \begin{matrix} V_{BE1} = V_{BE3} \\ V_{BE2} = V_{BE4} \end{matrix}$$

$$V_A = V_{in2} - V_{BE2} - V_{BE3}$$

$$V_B = V_{in1} - V_{BE1} - V_{BE4}$$

$$V_A - V_B = V_{in2} - V_{in1}$$



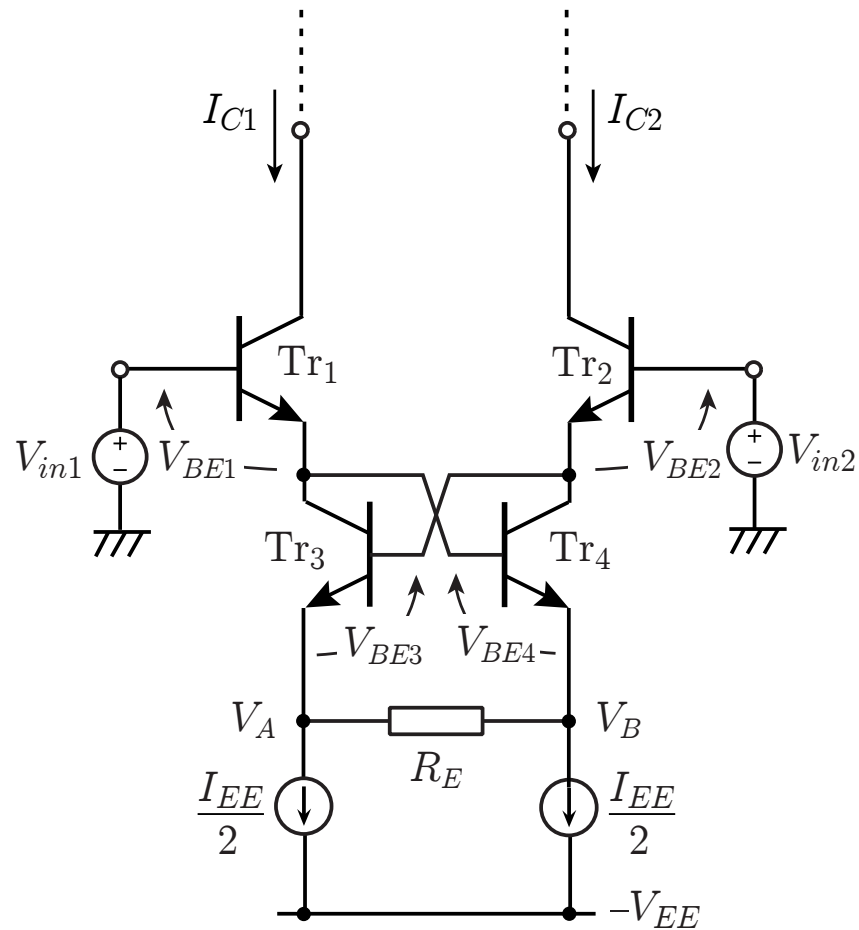
$$V_A - V_B = V_{in2} - V_{in1}$$

$$I_{RE} = \frac{V_{in2} - V_{in1}}{R_E} = \frac{-\Delta V_{in}}{R_E}$$

$$I_{C1} = \frac{I_{EE}}{2} + I_{RE}$$

$$I_{C2} = \frac{I_{EE}}{2} - I_{RE}$$

$$\Delta I_{out} = I_{C1} - I_{C2} = 2I_{RE} = \frac{-2}{R_E} \Delta V_{in}$$



Tr3について

$$V_{C3} = V_{in1} - V_{BE1}$$

$$V_{B3} = V_{in2} - V_{BE2}$$

$$V_{C3} > V_{B3} \rightarrow$$

$$V_{in1} - V_{BE1} > V_{in2} - V_{BE2}$$

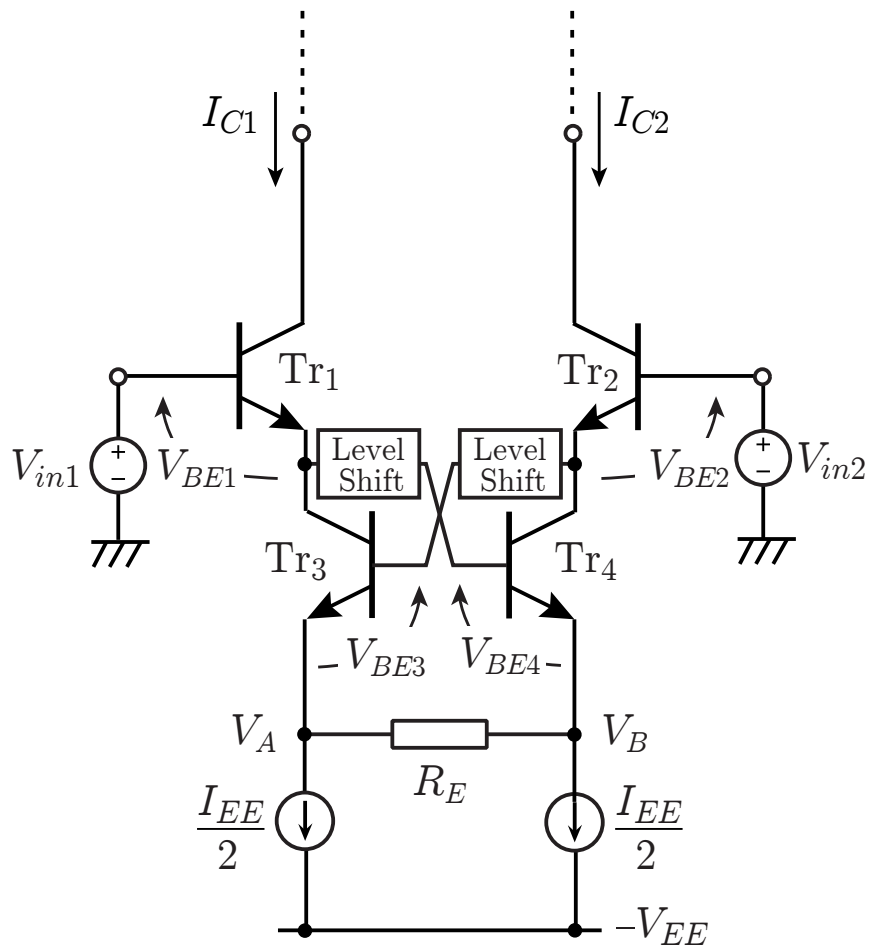
Tr4について

$$V_{C4} = V_{in2} - V_{BE2}$$

$$V_{B4} = V_{in1} - V_{BE1}$$

$$V_{C4} > V_{B4} \rightarrow$$

$$V_{in1} - V_{BE1} < V_{in2} - V_{BE2}$$



$$V_{C3}=V_{in1}-V_{BE1}$$

$$V_{B3}=V_{in2}-V_{BE2}-V_{shift}$$

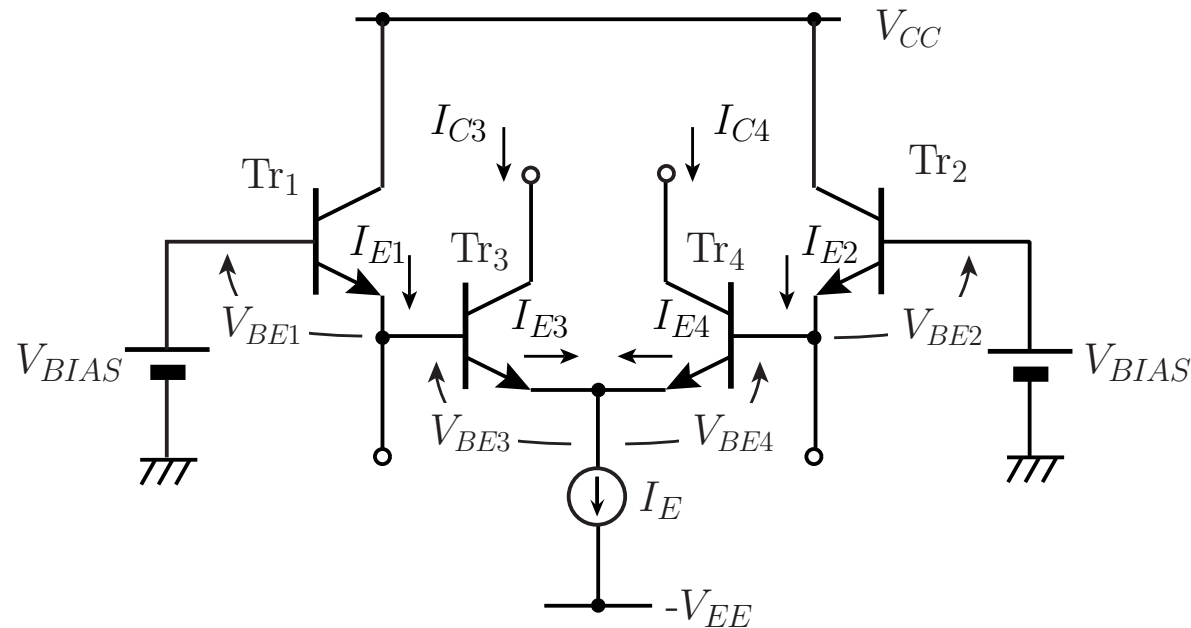
$$V_{in1}-V_{BE1}>V_{in2}-V_{BE2}-V_{shift}$$

$$V_{C4}=V_{in2}-V_{BE2}$$

$$V_{B4}=V_{in1}-V_{BE1}-V_{shift}$$

$$V_{in1}-V_{BE1}-V_{shift}<V_{in2}-V_{BE2}$$

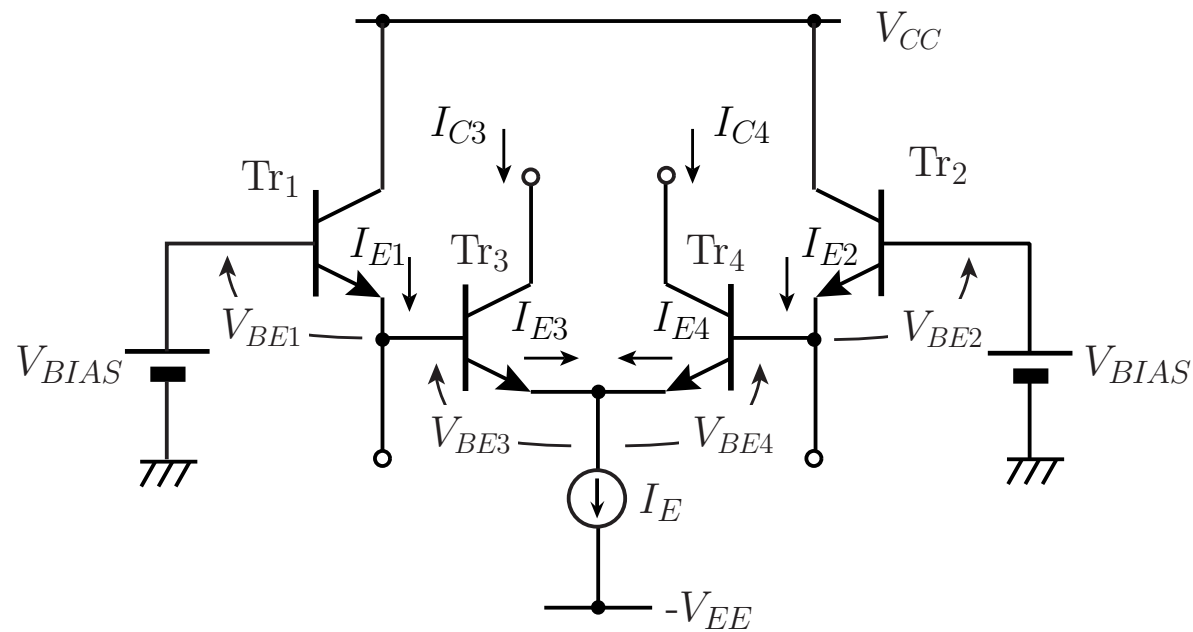
伝達コンダクタンスの電子的制御



$$V_{BE1} + V_{BE3} = V_{BE2} + V_{BE4}$$

$$\frac{kT}{q} \ln\left(\frac{I_{E1}}{I_{ES}}\right) + \frac{kT}{q} \ln\left(\frac{I_{E3}}{I_{ES}}\right) = \frac{kT}{q} \ln\left(\frac{I_{E2}}{I_{ES}}\right) + \frac{kT}{q} \ln\left(\frac{I_{E4}}{I_{ES}}\right)$$

$$I_{E1} I_{E3} = I_{E2} I_{E4}$$



$$I_{E3} + I_{E4} = I_E$$

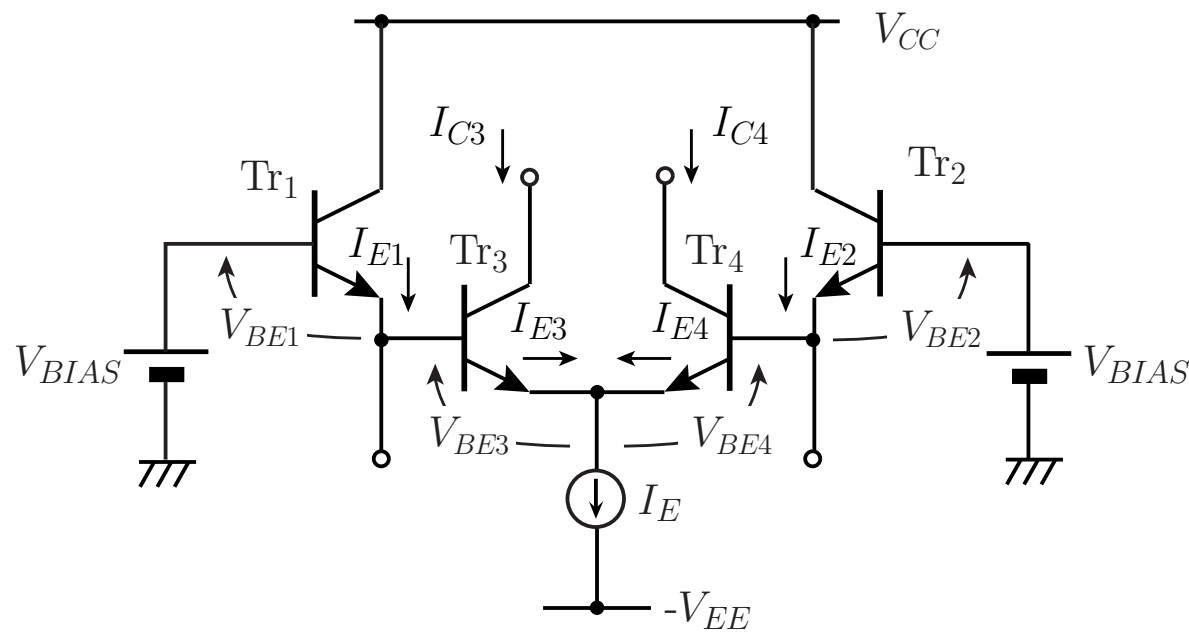
$$I_{E1} + I_{E2} = I_D \quad \longrightarrow \quad I_{E1} I_{E3} = I_{E2} I_{E4}$$

$$I_{E1} + I_{E2} = I_D$$

$$I_{E1} I_{E3} = (I_D - I_{E1})(I_E - I_{E3})$$

$$I_{E1} I_E + I_{E3} I_D = I_E I_D$$

$$\boxed{\frac{I_{E1}}{I_D} + \frac{I_{E3}}{I_E} = 1}$$



$$I_{E3} + I_{E4} = I_E$$

$$I_{E1} + I_{E2} = I_D$$

$$\frac{I_{E1}}{I_D} + \frac{I_{E3}}{I_E} = 1$$

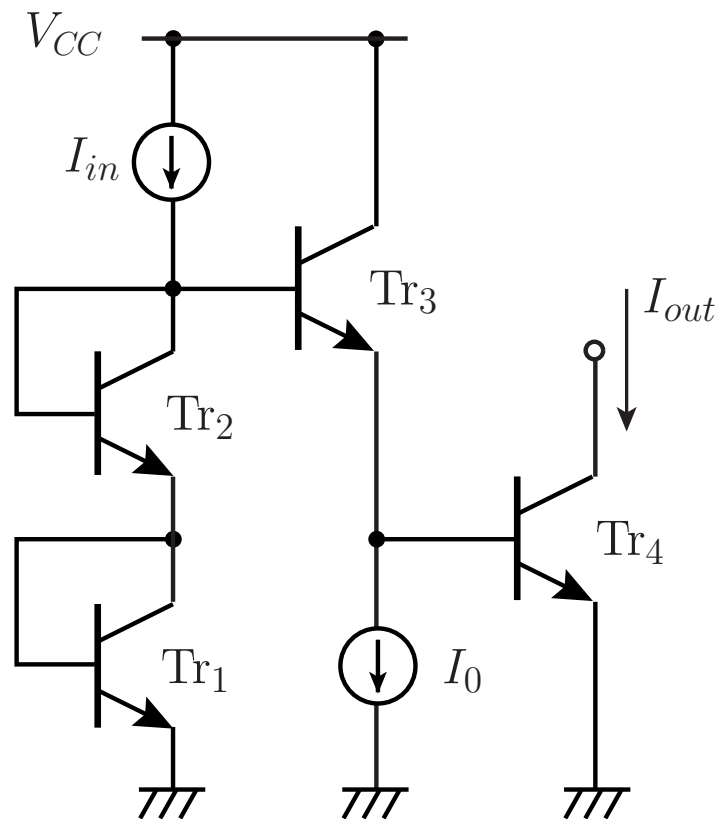
$$A_I = \frac{I_{C3} - I_{C4}}{I_{E1} - I_{E2}} = \frac{I_{E3} - I_{E4}}{I_{E1} - I_{E2}} = \frac{2I_{E3} - I_E}{2I_{E1} - I_D} = \frac{I_E}{I_D} \frac{2^{\frac{I_{E3}}{I_E}} - 1}{2^{\frac{I_{E1}}{I_D}} - 1}$$

$$A_I = \frac{I_E}{I_D} \frac{2^{\frac{I_{E3}}{I_E}} - 1}{2(1 - \frac{I_{E3}}{I_E}) - 1} = -\frac{I_E}{I_D}$$

問：バイポーラトランジスタのエミッタ電流が

$$I_E = I_S \exp \frac{qV_{BE}}{kT}$$

であり，コレクタ電流がエミッタ電流に等しいとき，
下図の回路の出力電流 I_{out} と入力電流 I_{in} の関係式を導出せよ．



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