## Nuclear Reactor Physics Lecture Note (5) - One-speed diffusion theory of a nuclear reactor (1) -

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5. One-speed diffusion theory of a nuclear reactor

5.1 The time-dependent "slab" reactor

(a)Solution of diffusion equation

Considering a uniform slab of fissile material characterized by cross sections  $\Sigma_a, \Sigma_{tr}, \Sigma_f$  (Slab reactor)

One-speed diffusion equation

$$\frac{1}{\nu}\frac{\partial \varphi}{\partial t} - D\frac{\partial^2 \varphi}{\partial x^2} + \Sigma_a \varphi(x,t) = \nu \Sigma_f \varphi(x,t) \qquad \cdots (1)$$

Initial condition

$$\phi(x,0) = \phi_0(x) = \phi_0(-x) \quad (symetric) \qquad \cdots (2)$$

Boundary conditions

$$\phi\left(\frac{\tilde{a}}{2},t\right) = \phi\left(-\frac{\tilde{a}}{2},t\right) = 0 \qquad \qquad \cdots (3)$$

solution of the form (separation variables)  

$$\phi(x,t) = \psi(x)T(t)$$
 ....(4)

Substituting Eq.(4) to Eq.(1) and dividing by  $\psi(x)T(t)$ 

$$\frac{1}{T}\frac{dT}{dt} = \frac{\nu}{\psi} \left[ D\frac{d^2\psi}{dx^2} + (\nu\Sigma_f - \Sigma_a)\psi(x) \right] = \text{constant} \equiv -\lambda \qquad \cdots (5)$$

hence

А

$$\frac{\mathrm{d}T}{\mathrm{d}t} = -\lambda T(t) \qquad \cdots (6)$$

$$D\frac{d^2\psi}{dx^2} + (\nu\Sigma_f - \Sigma_a)\psi(x) = -\frac{\lambda}{\nu}\psi(x) \qquad \cdots (7)$$

Solution of the time-dependent Eq.(6)

$$T(t) = T(0)e^{-\lambda t} \qquad \cdots (8)$$

Space dependent equation

$$D\frac{d^{2}\psi}{dx^{2}} + \left(\frac{\lambda}{\nu} + \nu\Sigma_{f} - \Sigma_{a}\right)\psi(x) = 0 \qquad \qquad \cdots (9)$$

Boundary condition

$$\psi\left(\frac{\tilde{a}}{2}\right) = \psi\left(-\frac{\tilde{a}}{2}\right) = 0 \qquad \cdots (10)$$

here  $\lambda$  is still to be determined.

Considering the eigenvalue problem.

$$\frac{d^2\psi}{dx^2} + B_m^2 \psi_n(x) = 0 \qquad \cdots (11)$$
$$\psi_n\left(\frac{\tilde{a}}{2}\right) = \psi_n\left(-\frac{\tilde{a}}{2}\right) = 0$$

We are interested in symmetric solutions since  $\,\varphi_0(x)\,$  is symmetric.

eigen functions :  $\psi_n(x) = \cos B_n x$ 

eigenvalue : 
$$B_n^2 = \left(\frac{n\pi}{\tilde{a}}\right)^2$$
,  $n = 1,3,5,\cdots$  ... (12)

If we identify Eq.(9) as the same problem, we must choose

$$\lambda = v\Sigma_{a} + vDB_{n}^{2} - vv\Sigma_{f} \equiv \lambda_{n}, \quad n = 1,3,5 \qquad \cdots (13)$$
  
$$\lambda_{n} : \text{time eigenvalues}$$

General solution of Eq.(1),

$$\phi(x,t) = \sum_{\substack{n \\ \text{odd}}} A_n \exp(-\lambda_n t) \cos \frac{n\pi x}{\tilde{a}} \qquad \cdots (14)$$

The solution satisfies the boundary conditions. From initial condition Eq.(2),

$$\phi(x,0) = \phi_0(x) = \sum_{\substack{n \\ \text{odd}}} A_n \cos \frac{n\pi x}{\tilde{a}} \qquad \cdots (15)$$

Using orthogonality,

$$A_{n} = \frac{2}{\tilde{a}} \int_{-\frac{\tilde{a}}{2}}^{\frac{\tilde{a}}{2}} dx \phi_{0}(x) \cos \frac{n\pi x}{\tilde{a}} \qquad \cdots (16)$$

Thus

$$\phi(\mathbf{x}, \mathbf{t}) = \sum_{\substack{n \\ \text{odd}}} \left[ \frac{2}{\tilde{a}} \int_{-\frac{\tilde{a}}{2}}^{\frac{\tilde{a}}{2}} d\mathbf{x}' \phi_0(\mathbf{x}') \cos B_n \mathbf{x}' \right] \exp(-\lambda_n \mathbf{t}) \cdot \cos B_n \mathbf{x} \qquad \cdots (17)$$

where the time eigenvalues  $\boldsymbol{\lambda}_n$  are given by

$$\lambda_n = v\Sigma_a + vDB_n^2 - vv\Sigma_f, \quad B_n = \frac{n\pi}{\tilde{a}}$$
 ... (18)

(b)Long time behavior

From Eq.(12)

$$B_1^2 < B_3^2 < \dots < B_n^2 = \left(\frac{n\pi}{\tilde{a}}\right)^2 \dots (19)$$

hence from Eq.(18)

$$\lambda_1 < \lambda_3 < \lambda_5 \cdots \cdots (20)$$

This means that the modes (terms in Eq.(17)) corresponding to larger n decay out rapidly in time.

as 
$$t \to \infty$$
  
 $\phi(x, t) \sim A_1 \exp(-\lambda, t) \cos B_1 x$  ... (21)  
(fundamental mode)

This shows the regardless of the initial shape  $\phi_0(x)$  the flux will decay into the fundamental mode shape.

It is usual to refer the value of  $B_n^{\ 2}$  characterizing this model as

$$B_1^2 = \left(\frac{\pi}{\tilde{a}}\right)^2 \equiv B_g^2 \equiv \text{geometric buckling} \qquad \cdots (22)$$

Thus nomenclature is used since  $B_n^2$  is a measure of the curvature of the mode shape  $B_n^2 = -\frac{1}{\psi_n} \frac{d^2 \psi_n}{dx^2}$ 

(c)Criticality condition

What is required to make the flux distribution in the reactor time-independent i.e. what is required to make the fission chain reaction steady-state We will define this situation to be that of reactor criticality :

Criticality  $\equiv$  when a time-independent neutron flux can be sustained in the reactor (in the absence of sources other than fissions)

The general solution of the flux

$$\phi(\mathbf{x}, \mathbf{t}) = A_1 \exp(-\lambda, \mathbf{t}) \cos B_1 \mathbf{x} + \sum_{\substack{n=3 \\ \text{odd}}}^{\infty} A_n \exp(-\lambda_n \mathbf{t}) \cos B_n \mathbf{x} \qquad \cdots (23)$$

It is evident that requirement for a time-independent flux is just that the fundamental eigenvalue vanish.

$$\lambda_1 = 0 = v(\Sigma_a - v\Sigma_f) + vDB_1^2 \qquad \cdots (24)$$

since then higher modes  $(n=3,5,\cdots)$  will have negative  $-\lambda_n$  and decay out in time, leaving just,

 $\phi(x, t) \rightarrow A_1 \cos B_1 \neq \text{function of time}$ 

From Eq.(24), using notation  $B_1^2 = B_g^2$ 

$$B_m^2 = B_g^2$$
 (criticality condition) ... (25)  
where,  $B_m^2 \equiv \frac{\nu \Sigma_f - \Sigma_a}{D}$  (material buckling) ... (26)

To achieve a critical reactor, we must either adjust the size  $(B_g^2)$  or the core composition  $(B_m^2)$  such that  $B_m^2 = B_g^2$ 

we also note,

$$\begin{split} &B_m^2 > B_g^{\ 2} \implies \lambda_1 < 0 \implies \text{super critical} \\ &B_m^2 = B_g^2 \implies \lambda_1 = 0 \implies \text{critical} \\ &B_m^2 < B_g^2 \implies \lambda_1 > 0 \implies \text{sub critical} \end{split}$$

$$B_{g}^{2} = \left(\frac{\pi}{\tilde{a}}\right)^{2}$$

$$B_{m}^{2} = \frac{\nu \Sigma_{f} - \Sigma_{a}}{D}$$

$$t \to \infty \qquad \varphi(x, t) \to A_{1} \exp(-\lambda_{1} t) \cdot \cos B_{g} x$$