

Structural Dynamics  
構造動力学  
(8)

Kazuhiko Kawashima  
Department of Civil Engineering  
Tokyo institute of Technology  
東京工業大学大学院理工学研究科土木工学専攻  
川島一彦

## 6.5 Equations of Motion for Undamped MDOF Systems in General Coordinate (基準座標で表した非減衰系の運動方程式)

- Assume to represent the response displacement vector (相対変位ベクトル) and the response acceleration vector (相対加速度ベクトル) as a linear combination of the mode shape vector (振動モードベクトル) and the generalized coordinate (一般化された座標)

$$\{u(x,t)\} = [\Phi(x)]\{q(t)\} \quad (6.34)$$

$$\{\ddot{u}(x,t)\} = [\Phi(x)]\{\ddot{q}(t)\}$$

where,

$\{q(t)\}$ : generalized coordinate (一般化された座標)

- Generalized coordinate (一般化された座標)  $\{q(t)\}$  is defined as

$$\{q(t)\} = \begin{Bmatrix} q_1(t) \\ q_2(t) \\ \vdots \\ q_i(t) \\ \vdots \\ q_n(t) \end{Bmatrix} \quad \{\ddot{q}(t)\} = \begin{Bmatrix} \ddot{q}_1(t) \\ \ddot{q}_2(t) \\ \vdots \\ \ddot{q}_i(t) \\ \vdots \\ \ddot{q}_n(t) \end{Bmatrix} \quad (6.35)$$

in which  $q_i(t)$  and  $\ddot{q}_i(t)$  represents displacement quantity and acceleration quantity associated with the i-th mode normalized by the mode shape

- Assuming undamped MDOF system with  $\ddot{u}_g = 0$  the equations of motion are written from Eq. (6.16) as

$$[M]\{\ddot{u}\} + [K]\{u\} = \{P\} \quad (6.36)$$

- Substituting Eq. (6.34), Eq. (6.36) becomes

$$[M][\Phi]\{\ddot{q}\} + [K][\Phi]\{q\} = \{P\} \quad (6.37)$$

$$[M]\{\ddot{u}\} + [K]\{u\} = \{P\} - \ddot{u}_g [M]\{I\} \quad (6.16)$$

$$\{u\} = [\Phi]\{q\} \quad (6.34)$$

$$\{\ddot{u}\} = [\Phi]\{\ddot{q}\}$$

- Recalling Eq. (6.25),

$$\begin{aligned}
 [\Phi] &= [\phi_1 \quad \phi_2 \quad \cdot \quad \cdot \quad \phi_n] \\
 &= \left[ \begin{array}{c|c|c|c|c} \phi_{11} & \phi_{12} & \cdot & \cdot & \phi_{1n} \\ \phi_{21} & \phi_{22} & \cdot & \cdot & \phi_{2n} \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ \phi_{n1} & \cdot & \cdot & \cdot & \phi_{nn} \end{array} \right] \quad (6.25) \\
 &\quad \phi_1 \quad \phi_2
 \end{aligned}$$

$[\Phi]\{q\}$  can be written as

$$[\Phi]\{q\} = \begin{bmatrix} \phi_{11} & \phi_{12} & \cdot & \cdot & \phi_{1n} \\ \phi_{21} & \phi_{22} & \cdot & \cdot & \phi_{2n} \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ \phi_{n1} & \cdot & \cdot & \cdot & \phi_{nn} \end{bmatrix} \begin{Bmatrix} q_1 \\ q_2 \\ \cdot \\ \cdot \\ q_n \end{Bmatrix}$$

$$\begin{aligned} &= \phi_{11}q_1 + \phi_{12}q_2 + \cdots + \phi_{1r}q_r + \cdots + \phi_{1n}q_n \\ &+ \phi_{21}q_1 + \phi_{22}q_2 + \cdots + \phi_{2r}q_r + \cdots + \phi_{2n}q_n \\ &\quad \vdots \\ &+ \phi_{r1}q_1 + \phi_{r2}q_2 + \cdots + \phi_{rr}q_r + \cdots + \phi_{rn}q_n \\ &\quad \vdots \\ &+ \phi_{n1}q_1 + \phi_{n2}q_2 + \cdots + \phi_{nr}q_r + \cdots + \phi_{nn}q_n^6 \end{aligned}$$

•  $[\Phi]\{q\}$  can be arranged as

$$\begin{aligned}
 [\Phi]\{q\} = & \phi_{11}q_1 + \phi_{12}q_2 + \cdots + \phi_{1r}q_r + \cdots + \phi_{1n}q_n \\
 & + \phi_{21}q_1 + \phi_{22}q_2 + \cdots + \phi_{2r}q_r + \cdots + \phi_{2n}q_n \\
 & \vdots \\
 & + \phi_{r1}q_1 + \phi_{r2}q_2 + \cdots + \phi_{rr}q_r + \cdots + \phi_{rn}q_n \\
 & \vdots \\
 & + \phi_{n1}q_1 + \phi_{n2}q_2 + \cdots + \phi_{nr}q_r + \cdots + \phi_{nn}q_n
 \end{aligned}$$

$\{\phi_1\}$  ←

$$= \begin{Bmatrix} \phi_{11} \\ \vdots \\ \phi_{i1} \\ \vdots \\ \phi_{n1} \end{Bmatrix} q_1(t) + \begin{Bmatrix} \phi_{12} \\ \vdots \\ \phi_{i2} \\ \vdots \\ \phi_{n2} \end{Bmatrix} q_2(t) + \cdots + \begin{Bmatrix} \phi_{1n} \\ \vdots \\ \phi_{in} \\ \vdots \\ \phi_{nn} \end{Bmatrix} q_n(t)$$

- Hence,

$$[\Phi]\{q\} = \{\phi_1\}q_1 + \{\phi_2\}q_2 + \cdots \cdots \cdots \{\phi_r\}q_r + \cdots \cdots \cdots \{\phi_n\}q_n$$

(6.38)

- Similarly,

$$[\Phi]\{\ddot{q}\} = \{\phi_1\}\ddot{q}_1 + \{\phi_2\}\ddot{q}_2 + \cdots \cdots \cdots \{\phi_r\}\ddot{q}_r + \cdots \cdots \cdots \{\phi_n\}\ddot{q}_n$$

(6.39)



- Premultiplying  $\{\phi_r\}^T$  to Eq. (6.37),

$$\{\phi_r\}^T [M][\Phi]\{\ddot{q}\} + \{\phi_r\}^T [K][\Phi]\{q\} = \{\phi_r\}^T \{P\}$$

- Then substitution of Eq. (6.25) leads to

$$\begin{aligned} & \{\phi_r\}^T [M][\phi_1 \quad \phi_2 \quad \cdot \quad \cdot \quad \phi_r \quad \cdot \quad \cdot \quad \phi_n]\{\ddot{q}\} \\ & + \{\phi_r\}^T [K][\phi_1 \quad \phi_2 \quad \cdot \quad \cdot \quad \phi_r \quad \cdot \quad \cdot \quad \phi_n]\{q\} = \{\phi_r\}^T \{P\} \end{aligned} \quad (6.40)$$

- From the orthogonal condition by Eq. (6.33),

$$[\Phi] = [\phi_1 \quad \phi_2 \quad \cdot \quad \cdot \quad \phi_n] \quad (6.25)$$

$$\{\phi_r\}^T [M]\{\phi_s\} = 0 \quad (6.33a)$$

$$\{\phi_r\}^T [K]\{\phi_s\} = 0 \quad (6.33b)$$

$$[M][\Phi]\{\ddot{q}\} + [K][\Phi]\{q\} = \{P\} \quad (6.37)$$

Eq. (6.40) becomes

$$\{\phi_r\}^T [M] \{\phi_r\} \ddot{q}_r + \{\phi_r\}^T [K] \{\phi_r\} q_r = \{\phi_r\}^T \{P\} \quad (6.41)$$

because all the term  $\{\phi_r\}^T [M] \{\phi_s\}$  ( $r \neq s$ ) vanish.

- Representing

$$M_r^* = \{\phi_r\}^T [M] \{\phi_r\} \quad (6.42a)$$

$$K_r^* = \{\phi_r\}^T [K] \{\phi_r\} \quad (6.42b)$$

$$P_r^* = \{\phi_r\}^T \{P\} \quad (6.42c)$$

$$\begin{aligned} & \{\phi_r\}^T [M] [\phi_1 \quad \phi_2 \quad \cdot \quad \cdot \quad \phi_r \quad \cdot \quad \cdot \quad \phi_n] \{\ddot{q}\} \\ & + \{\phi_r\}^T [K] [\phi_1 \quad \phi_2 \quad \cdot \quad \cdot \quad \phi_r \quad \cdot \quad \cdot \quad \phi_n] \{q\} = \{\phi_r\}^T \{P\} \end{aligned} \quad (6.40)$$

Eq. (6.41) can be expressed

$$M_r^* \ddot{q}_r + K_r^* q_r = P_r^* \quad (6.43)$$

in which  $M_r^*$ ,  $K_r^*$  and  $P_r^*$  are called **generalized mass, generalized stiffness and generalized force of the r-th mode** (一般化されたr次の質量、一般化されたr次のばね定数、一般化されたr次の荷重).

- Eq. (6.43) is an uncoupled equation of the SDOF system representing the dynamic equilibrium for the r-th mode of the system.
- A similar independent equation may be written for each of the n-modes of oscillation.

$$\{\phi_r\}^T [M] \{\phi_r\} \ddot{q} + \{\phi_r\}^T [K] \{\phi_r\} q = \{\phi_r\}^T \{P\} \quad (6.41)^{11}$$

- It is emphasized that n-th coupled dynamic equations of motion of MDOF system with n degree-of-freedom system (Eq. (6.41))(n自由度を持つ連成した運動方程式) was decoupled into n-sets of dynamic equation of motion of SDOF system (n個の連成していない(非連成)の1自由度系の運動方程式に分解できた) using the orthogonal condition (直交条件).
- This is the great advantage of using the orthogonal condition.

$$\{\phi_r\}^T [M] \{\phi_r\} \ddot{q}_r + \{\phi_r\}^T [K] \{\phi_r\} q_r = \{\phi_r\}^T \{P\} \quad (6.41)$$

$$M_r^* \ddot{q}_r + K_r^* q_r = P_r^* \quad (6.43)$$

- From Eqs. (6.42) and (6.43), one obtains the r-th angular natural frequency as

$$\omega_r = \sqrt{\frac{K_r^*}{M_r^*}} = \sqrt{\frac{\{\phi_r\}^T [K] \{\phi_r\}}{\{\phi_r\}^T [M] \{\phi_r\}}} \quad (6.44)$$

$$M_r^* = \{\phi_r\}^T [M] \{\phi_r\} \quad (6.42a)$$

$$K_r^* = \{\phi_r\}^T [K] \{\phi_r\} \quad (6.42b)$$

$$M_r^* \ddot{q}_r + K_r^* q_r = P_r^* \quad (6.43)$$