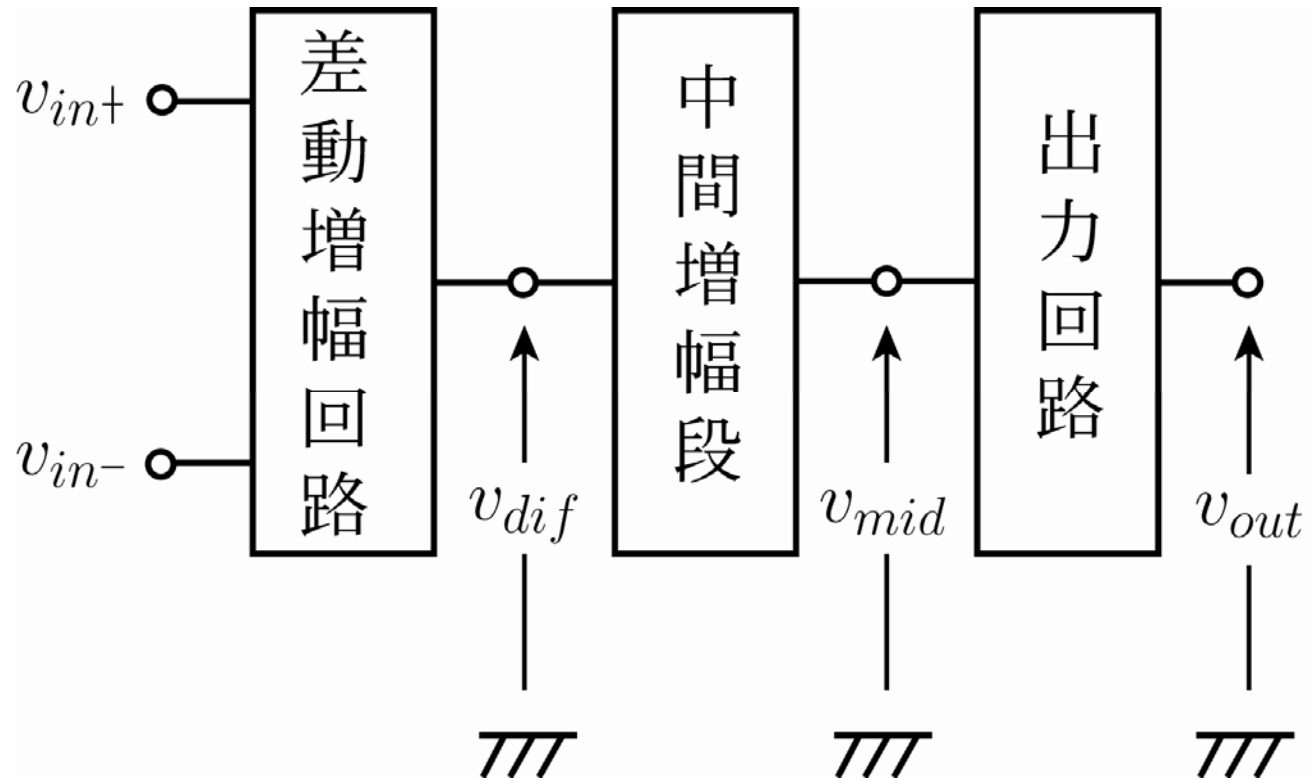
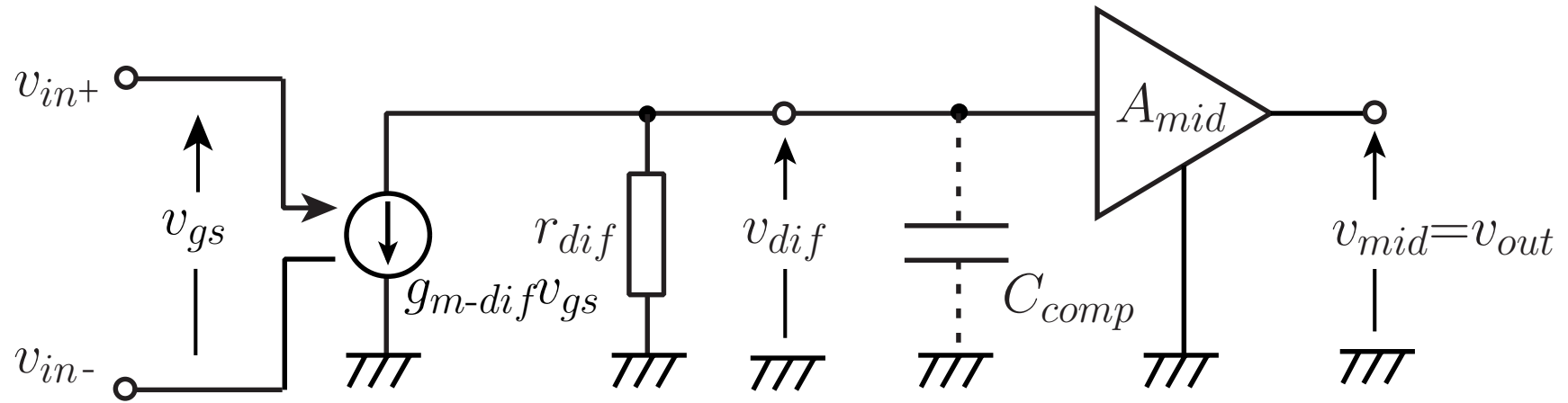


演算増幅器

演算増幅器の基本構成



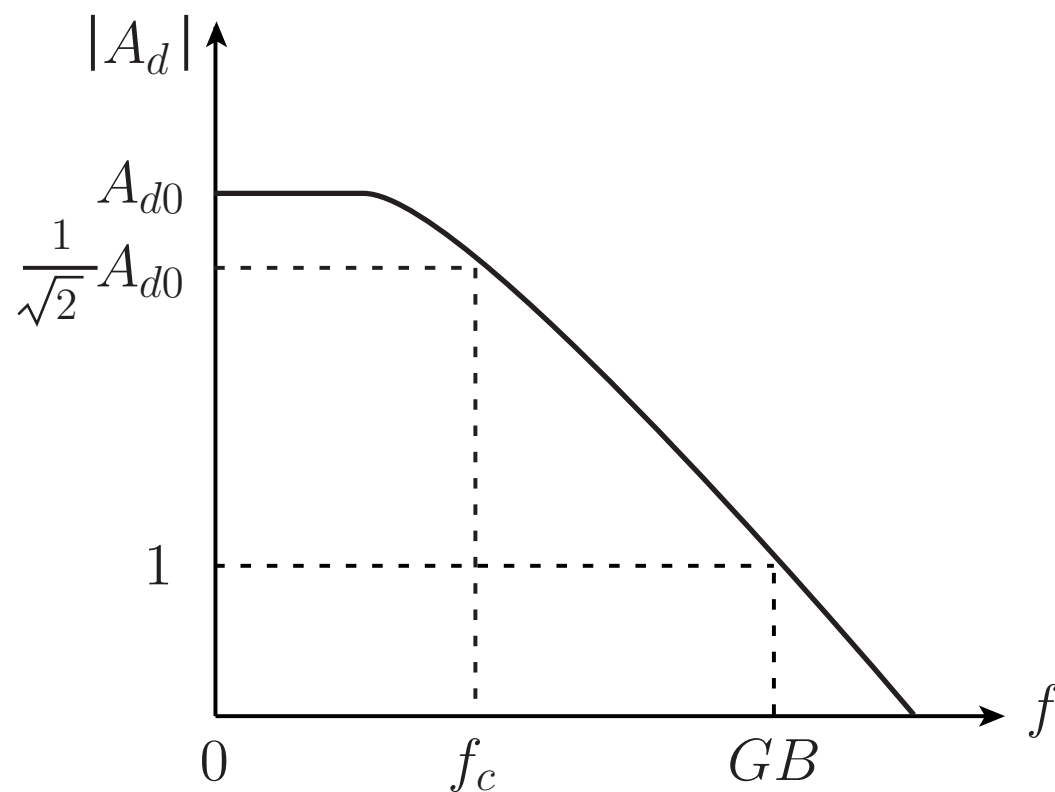
基本演算増幅器の近似モデル



問 v_{out} と v_{in+} , v_{in-} の関係を示せ.

$$A_d = A_{\text{mid}} \frac{g_{\text{m-dif}} r_{\text{dif}}}{1 + s C_{\text{comp}} r_{\text{dif}}} = \frac{A_{d0}}{1 + j \frac{f}{f_c}}$$

$$\frac{f}{f_c} \gg 1 \text{ と仮定} \quad |A_d| \approx \frac{A_{d0} f_c}{f} \quad \Rightarrow 1 \rightarrow f = A_{d0} f_c = GB$$

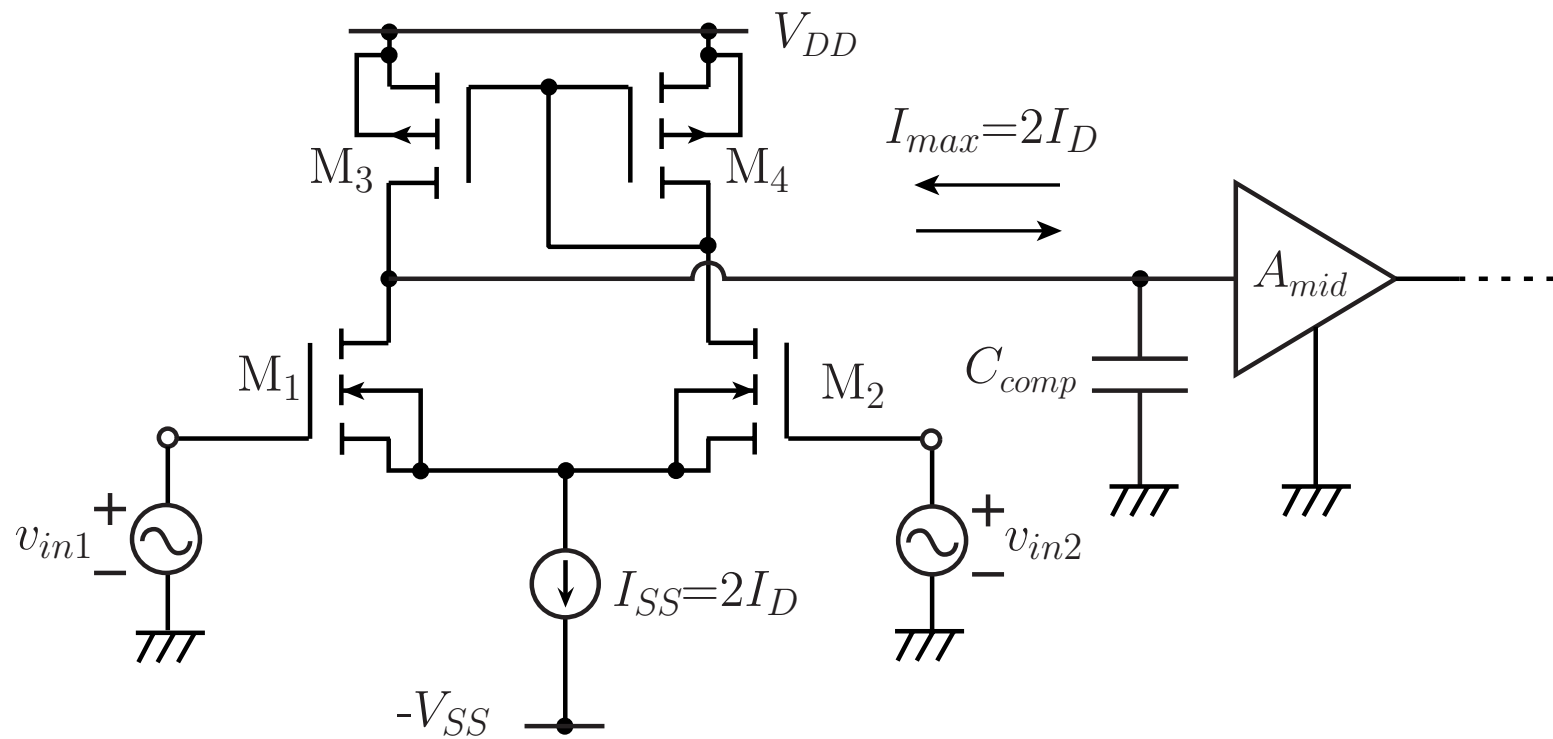


$$A_d = A_{\text{mid}} \frac{g_{\text{m-dif}} r_{\text{dif}}}{1 + s C_{\text{comp}} r_{\text{dif}}} = \frac{A_{\text{d0}}}{1 + j \frac{f}{f_c}}$$

問 $g_{\text{m-dif}} \approx 2\sqrt{K I_D}$, $I_D \approx \frac{1}{\lambda V_{\text{DS}}}$ という関係を用いて
直流利得 A_{d0} を求めよ.

$$A_d = A_{mid} \frac{g_{m-dif} r_{dif}}{1 + s C_{comp} r_{dif}} = \frac{A_{d0}}{1 + j \frac{f}{f_c}}$$

問 $g_{m-dif} \approx 2\sqrt{K I_D}$, $I_D \approx \frac{1}{\lambda V_{DS}}$ という関係を用いて
利得帯域幅積GBを求めよ.



問 C_{comp} の両端に生じる電圧について,
単位時間あたりの最大の変化量SRを求めよ.

特性のトレードオフ

$$A_{d0} = A_{\text{mid}} g_{\text{m-dif}} r_{\text{dif}} \approx A_{\text{mid}} \frac{2}{\lambda} \sqrt{\frac{K}{I_D}}$$

$$GB = \frac{A_{\text{mid}} g_{\text{m-dif}}}{2\pi C_{\text{comp}}} \approx \frac{A_{\text{mid}} \sqrt{K I_D}}{\pi C_{\text{comp}}}$$

$$SR = \frac{2I_D}{C_{\text{comp}}} \approx \frac{g_{\text{m-dif}}^2}{2KC_{\text{comp}}}$$

バイポーラトランジスタを用いた 演算増幅器の場合

$$g_{m-dif} \approx \frac{\alpha_0 q I_E}{kT} \quad r_{dif} \approx \frac{V_A}{I_C} = \frac{V_A}{\alpha_0 I_E}$$

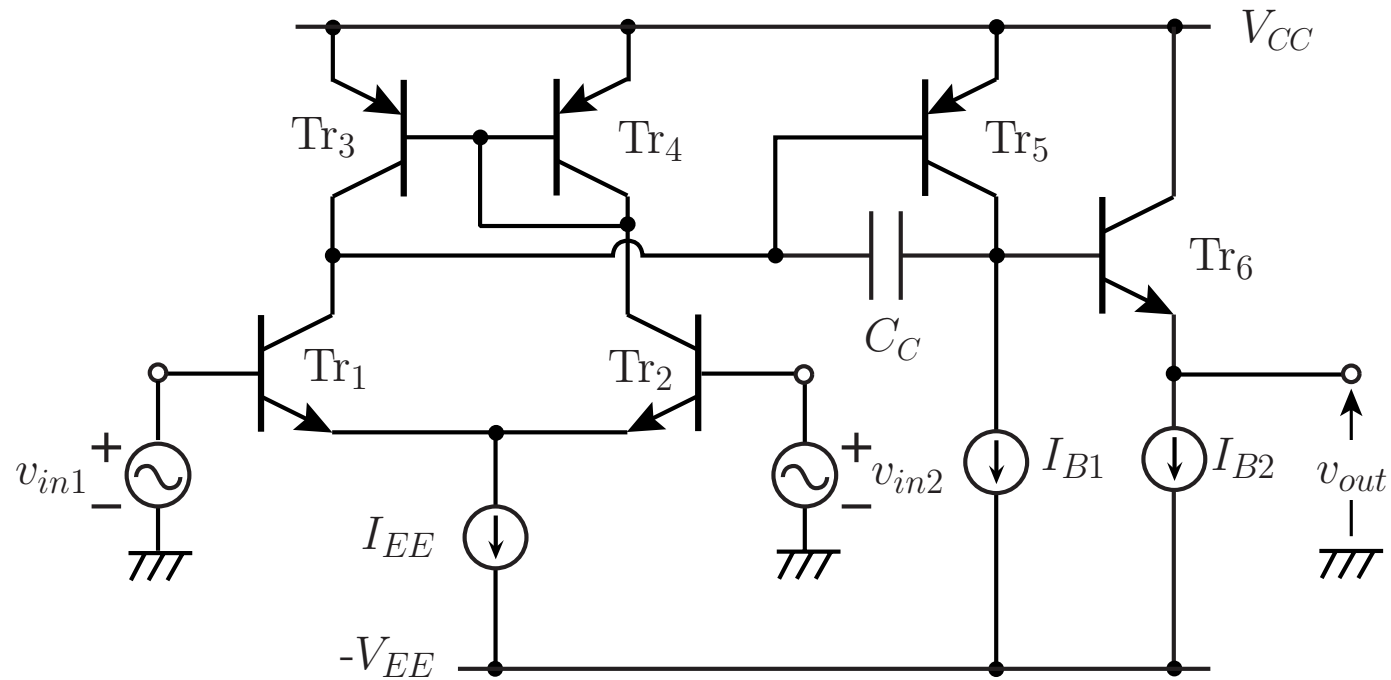
$$A_{d0} = A_{mid} g_{m-dif} r_{dif} \approx A_{mid} \frac{q V_A}{kT}$$

$$GB = \frac{A_{mid} g_{m-dif}}{2\pi C_{comp}} = \frac{A_{mid} \alpha_0 q I_E}{2\pi C_{comp} kT}$$

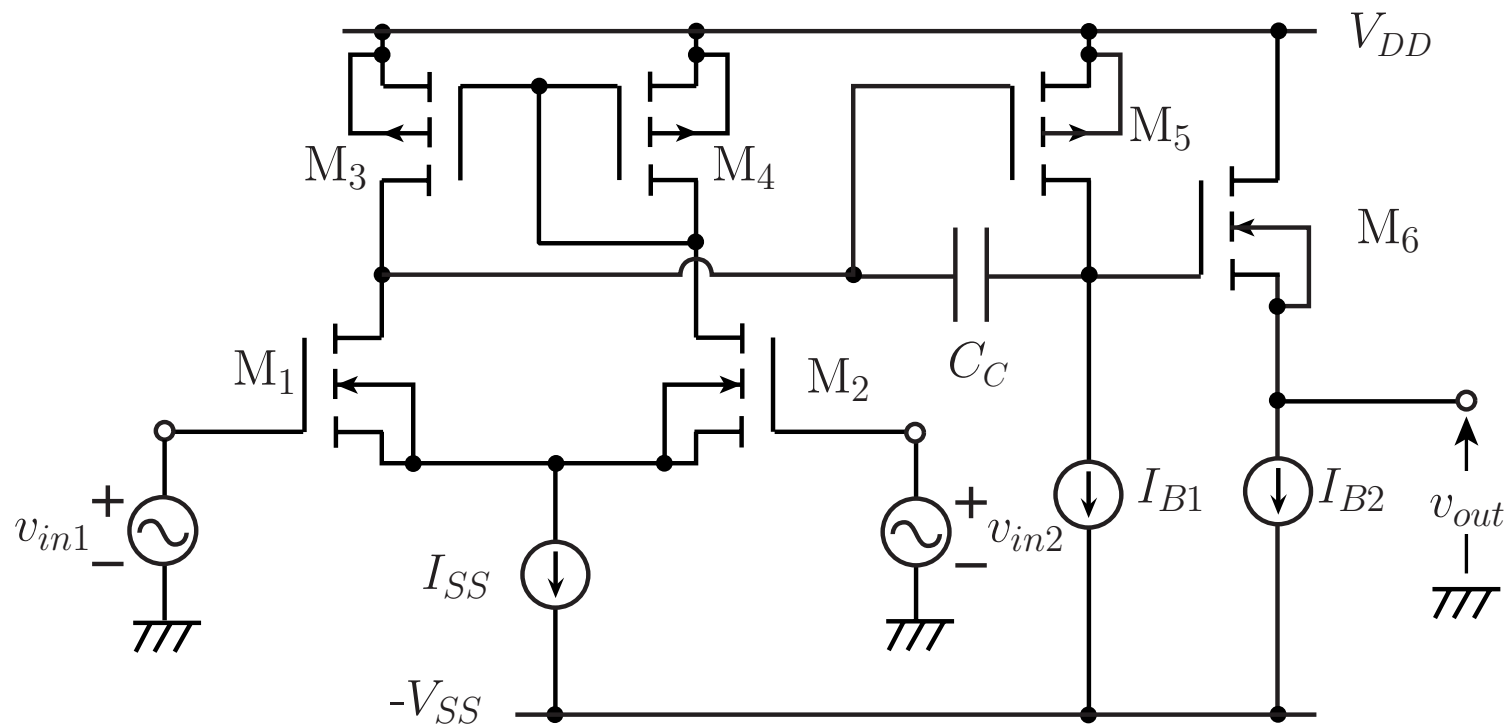
$$SR = \frac{2\alpha_0 I_E}{C_{comp}} = \frac{2kT g_{m-dif}}{q C_{comp}} = \frac{4\pi GB}{q}$$

演算増幅器の構成例

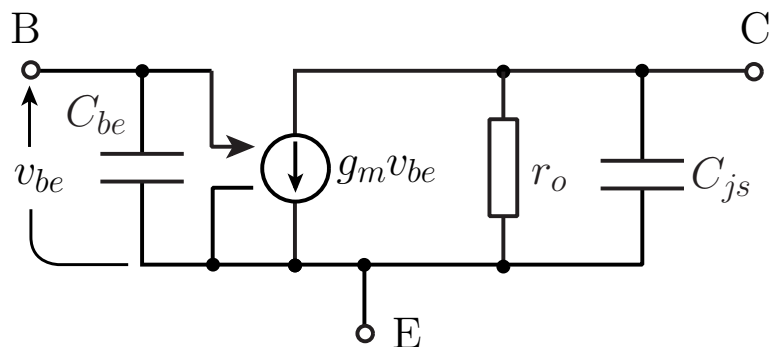
バイポーラトランジスタによる演算増幅器の構成例



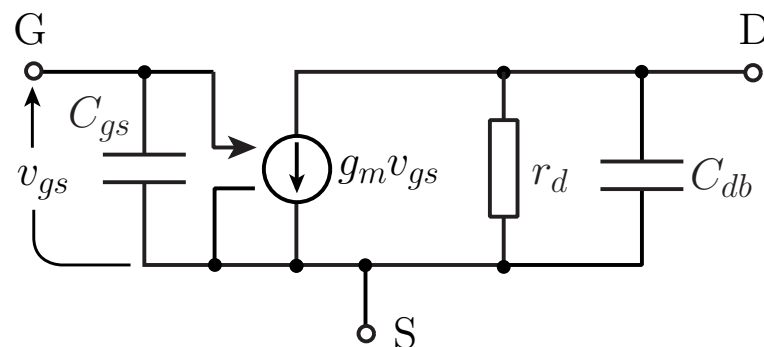
MOSトランジスタによる演算増幅器の構成例



トランジスタのモデル

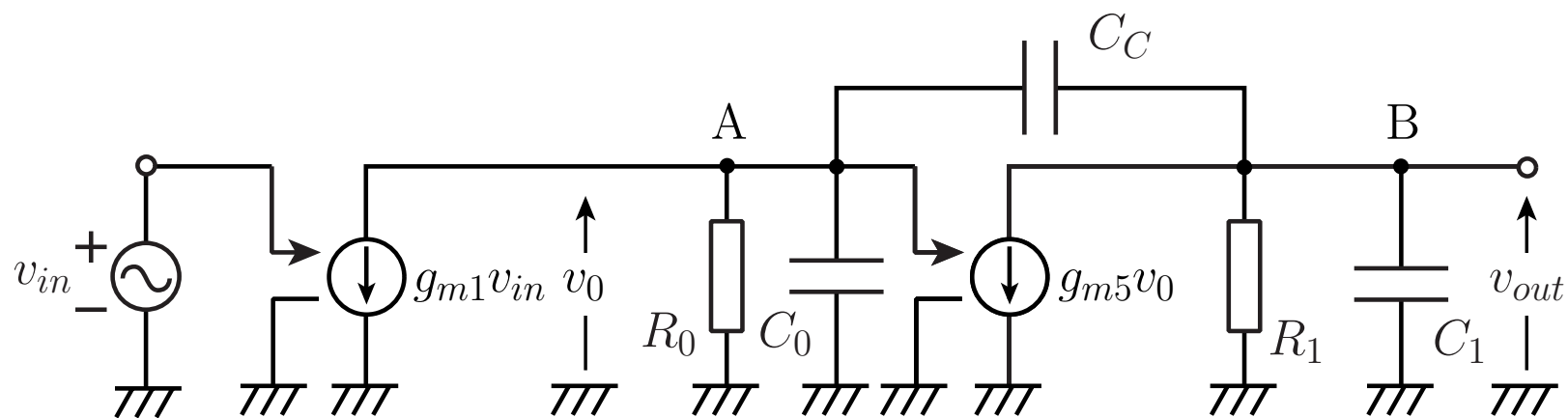
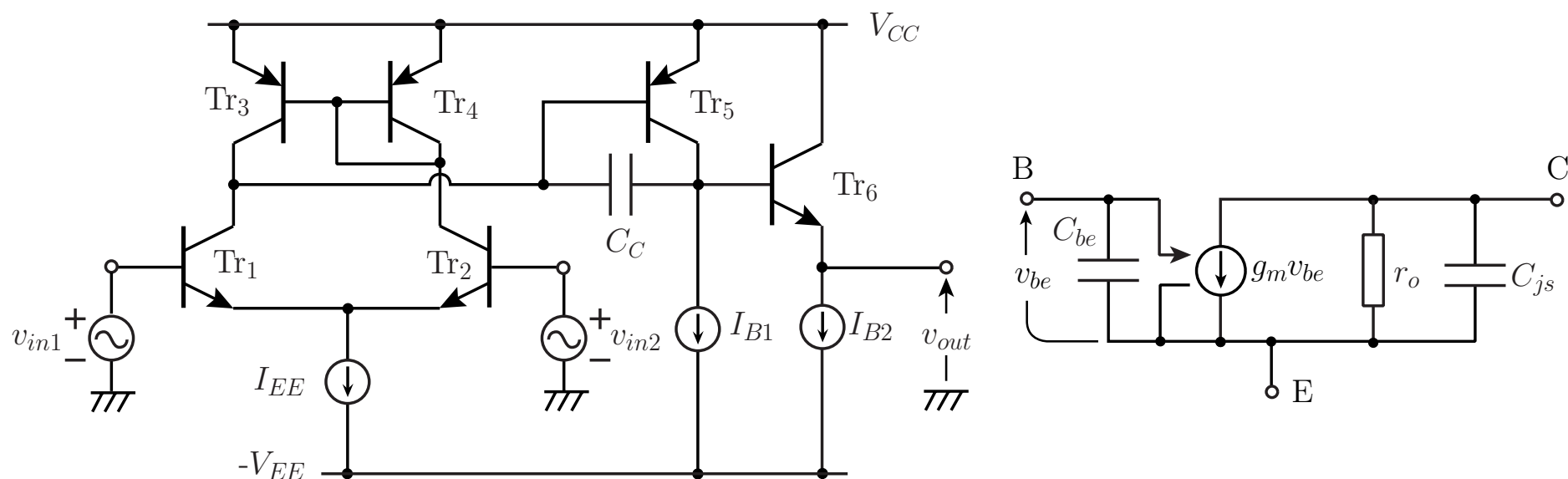


バイポーラトランジスタ

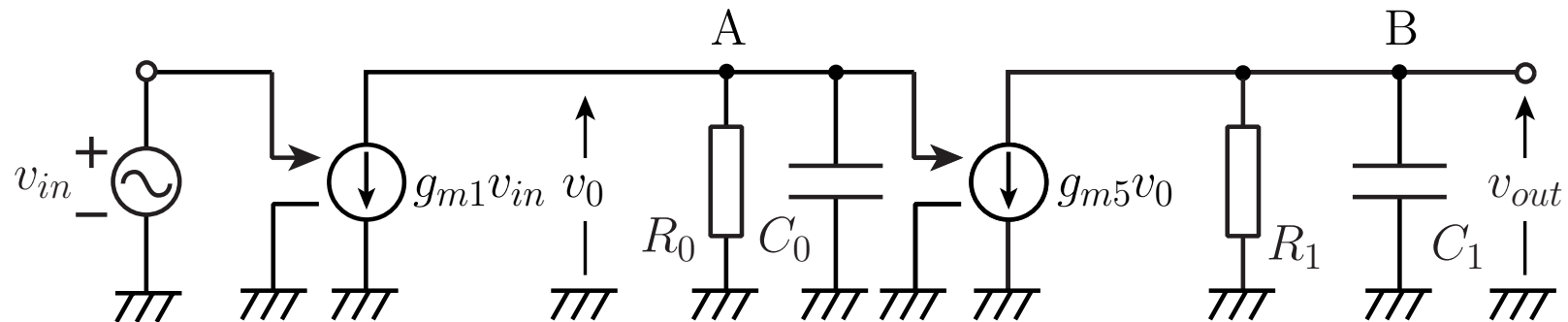


MOSトランジスタ

演算増幅器のモデル



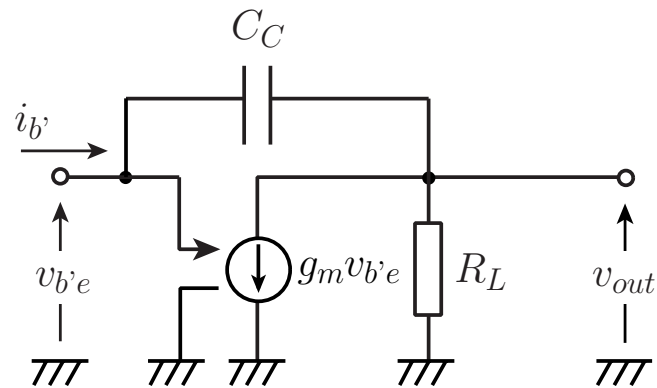
$C_C = 0$ のとき（零時定数解析）



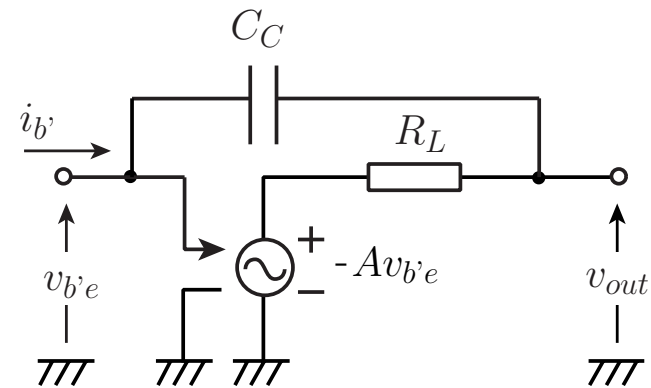
$$\tau_A = C_0 R_0$$

$$\tau_B = C_1 R_1$$

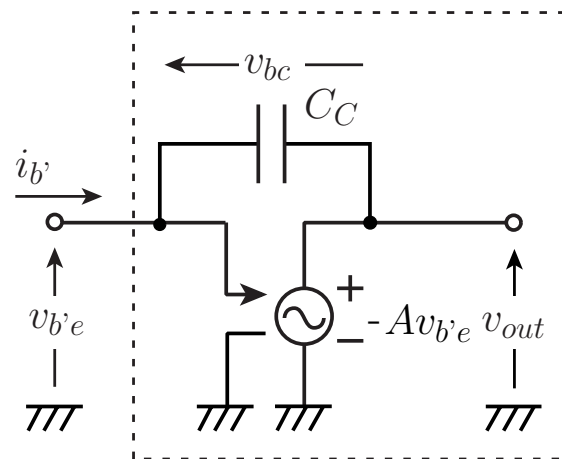
$C_C \neq 0$ のとき（零時定数解析）



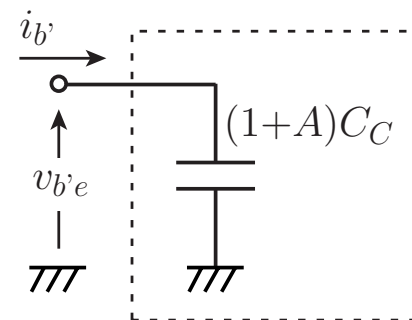
(a)



(b)

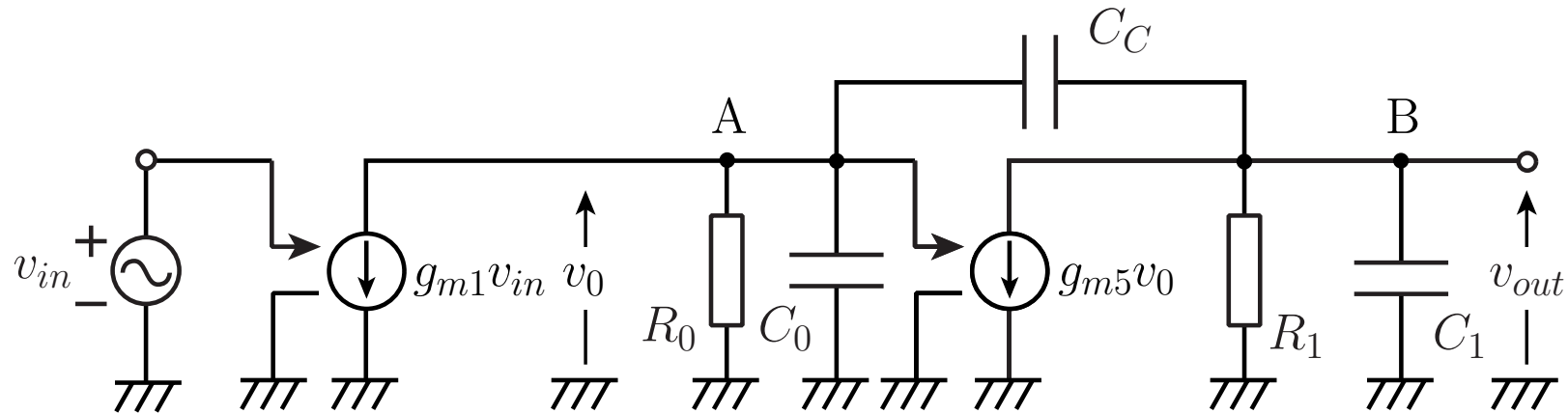


(c)



(d)

$C_C \neq 0$ のとき（零時定数解析）

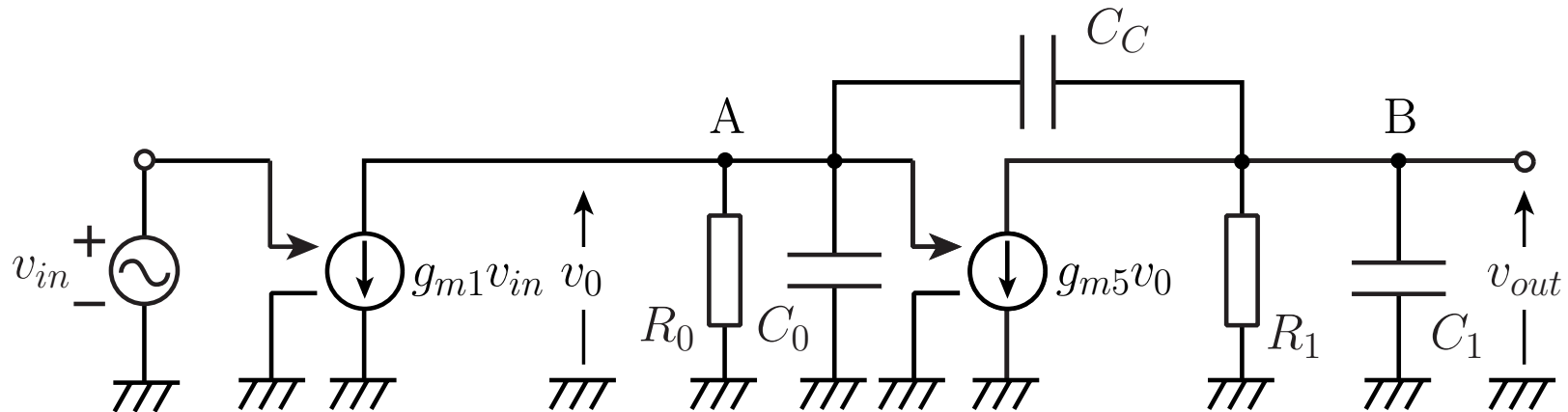


$$\tau_A' = \{C_0 + C_C(1 + g_{m5}R_1)\}R_0$$

$$R_{fb} = \frac{1}{\frac{C_C}{C_0 + C_C}g_{m5}} = \frac{C_0 + C_C}{C_C g_{m5}}$$

$$\tau_B' = \left(C_1 + \frac{C_0 C_C}{C_0 + C_C}\right) \frac{R_1 R_{fb}}{R_1 + R_{fb}}$$

差動利得の解析



$$A_d = \frac{g_{m1} R_0 R_1 (g_{m5} - s C_C)}{D(s)}$$

$$D(s) = 1 + s \{ C_C (R_0 + R_1 + g_{m5} R_0 R_1) + C_0 R_0 + C_1 R_1 \} \\ + s^2 (C_C C_0 + C_0 C_1 + C_1 C_C) R_0 R_1$$

$$A_d = A_{d0} \frac{1 - \frac{s}{z_1}}{\left(1 - \frac{s}{p_1}\right)\left(1 - \frac{s}{p_2}\right)} \approx A_{d0} \frac{1 - \frac{s}{z_1}}{1 - \frac{s}{p_1} + \frac{s^2}{p_1 p_2}}$$

$$A_d = \frac{g_{m1} R_0 R_1 (g_{m5} - s C_C)}{D_{Ad}(s)}$$

$$D(s) = 1 + s \{ C_C (R_0 + R_1 + g_{m5} R_0 R_1) + C_0 R_0 + C_1 R_1 \} \\ + s^2 (C_C C_0 + C_0 C_1 + C_1 C_C) R_0 R_1$$

$$A_d = \frac{g_{m1}R_0R_1(g_{m5} - sC_C)}{D_{Ad}(s)}$$

$$D_{Ad}(s) = 1 + s\{C_C(R_0 + R_1 + g_{m5}R_0R_1) + C_0R_0 + C_1R_1\} \\ + s^2(C_C C_0 + C_0 C_1 + C_1 C_C)R_0R_1$$

$$A_{d0} = g_{m1}R_0R_1g_{m5}$$

$$z_1 = \frac{g_{m5}}{C_C}$$

$$p_1 = \frac{-1}{C_C(R_0 + R_1 + g_{m5}R_0R_1) + C_0R_0 + C_1R_1}$$

$$p_2 = \frac{-\{C_C(R_0 + R_1 + g_{m5}R_0R_1) + C_0R_0 + C_1R_1\}}{(C_C C_0 + C_0 C_1 + C_1 C_C)R_0R_1}$$

零時定数と極の比較

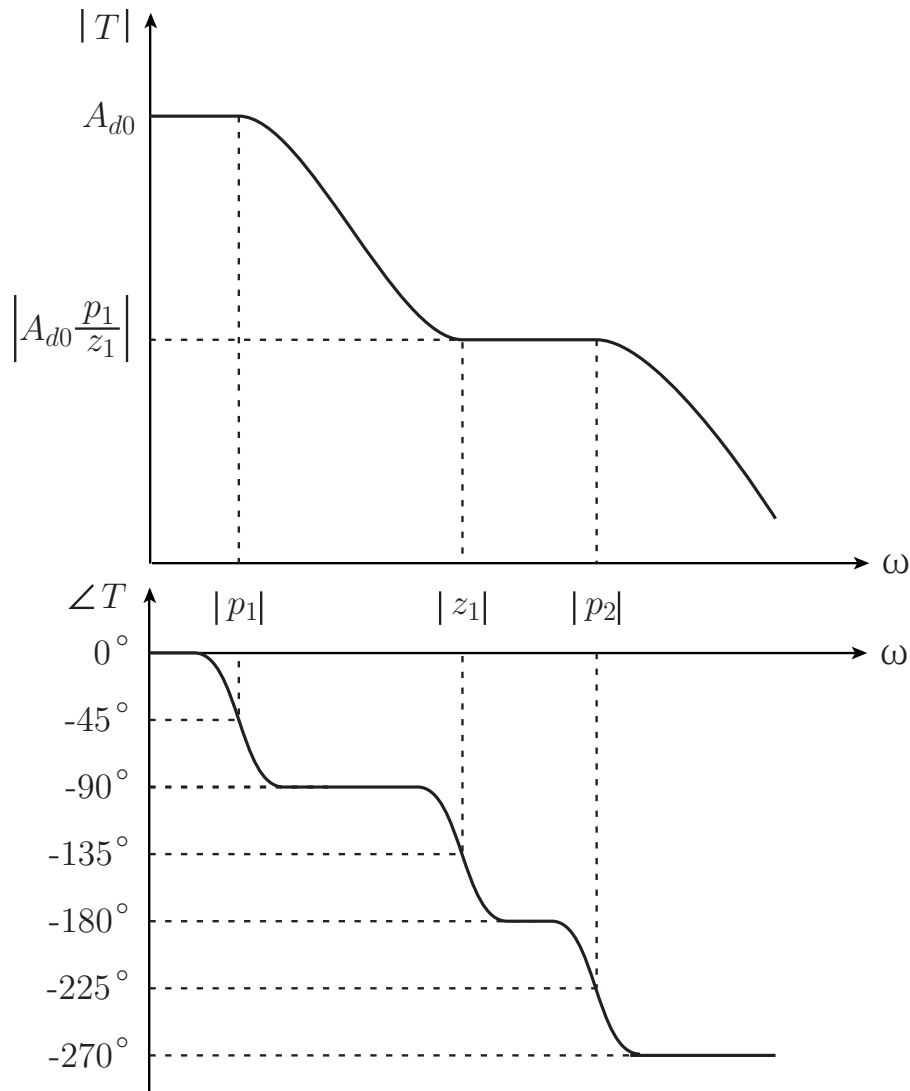
$$p_1 = \frac{-1}{C_C(R_0 + R_1 + g_{m5}R_0R_1) + C_0R_0 + C_1R_1} \approx \frac{-1}{C_C g_{m5}R_0R_1}$$

$$\tau_A' = \{C_0 + C_C(1 + g_{m5}R_1)\}R_0 \approx C_C g_{m5}R_0R_1$$

$$p_2 = \frac{-\{C_C(R_0 + R_1 + g_{m5}R_0R_1) + C_0R_0 + C_1R_1\}}{(C_C C_0 + C_0 C_1 + C_1 C_C)R_0R_1} \approx \frac{-g_{m5}}{C_0 + C_1}$$

$$\begin{aligned} \tau_B' &= \left(C_1 + \frac{C_0 C_C}{C_0 + C_C}\right) \frac{R_1 R_{fb}}{R_1 + R_{fb}} \\ &\approx \left(C_1 + \frac{C_0 C_C}{C_0 + C_C}\right) R_{fb} = \left(\frac{C_1 C_0 + C_1 C_C + C_0 C_C}{C_0 + C_C}\right) \frac{C_0 + C_C}{C_C g_{m5}} \\ &\approx \frac{C_1 + C_0}{g_{m5}} \end{aligned}$$

$$A_{d0} = g_{m1} R_0 R_1 g_{m5} \quad z_1 = \frac{g_{m5}}{C_C} \quad p_1 \approx \frac{-1}{C_C g_{m5} R_0 R_1} \quad p_2 \approx \frac{-g_{m5}}{C_0 + C_1}$$



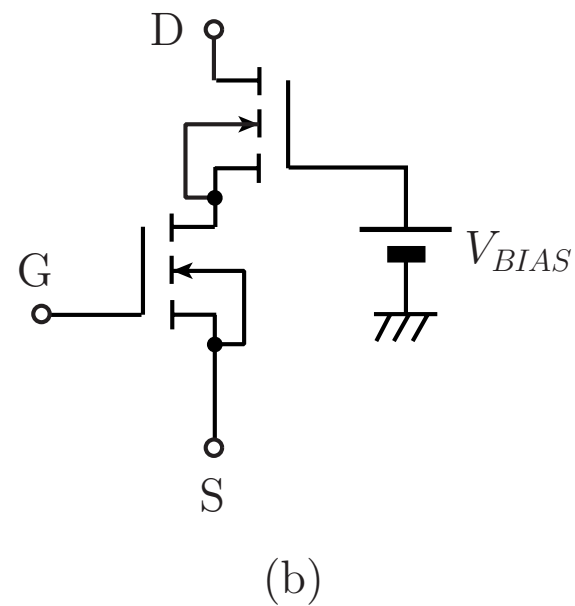
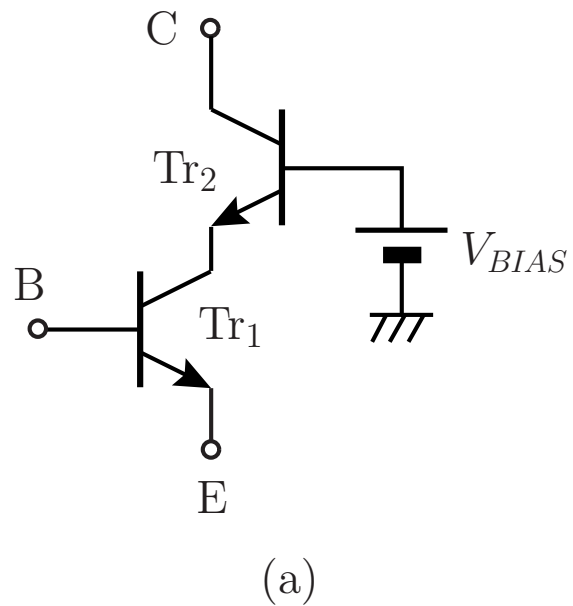
$$A_d = \frac{g_{m1} R_0 R_1 (g_{m5} - s C_C)}{D_{Ad}(s)}$$



$$A_d = \frac{g_{m1} R_0 R_1 (g_{m5} - \frac{s C_C}{1 + s C_C R_C})}{D_{Ad}(s)}$$

$$z_1 = \frac{g_{m5}}{C_C (1 - g_{m5} R_C)}$$

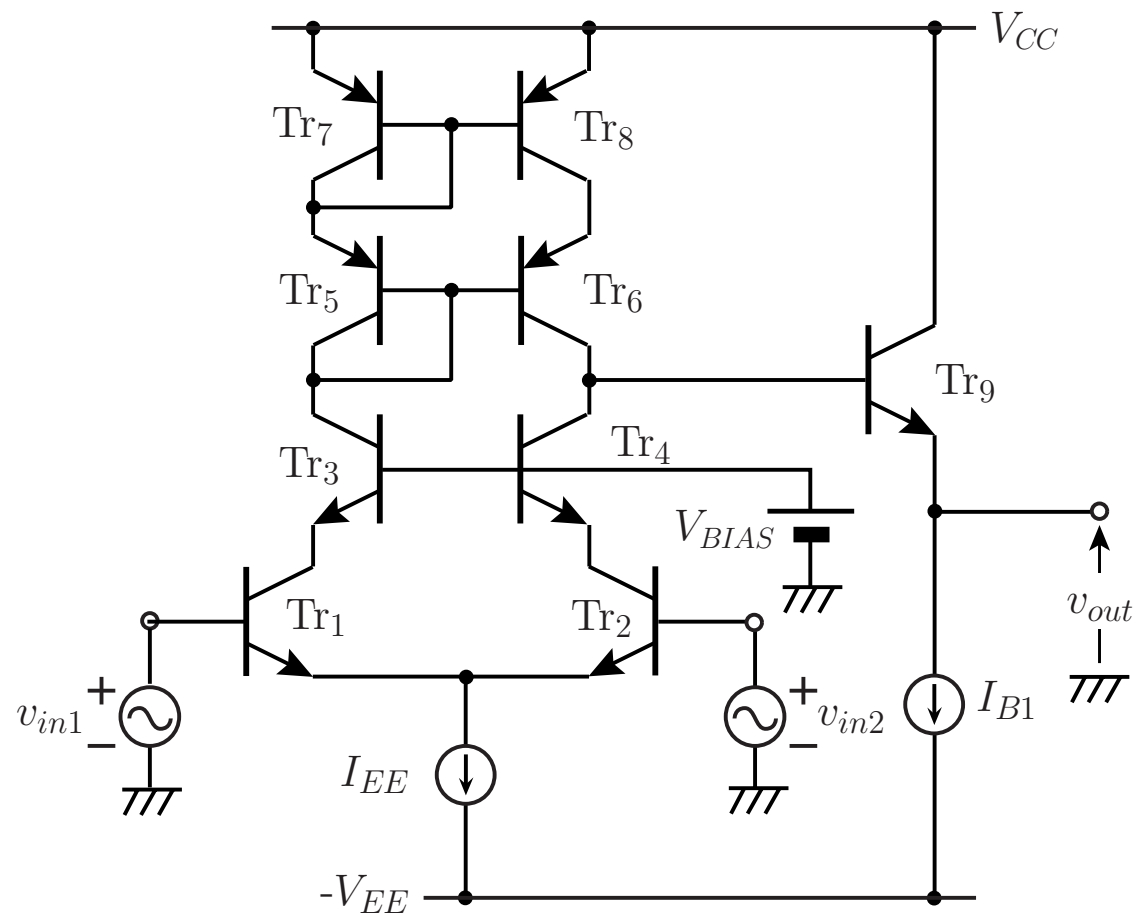
カスコード型演算増幅器



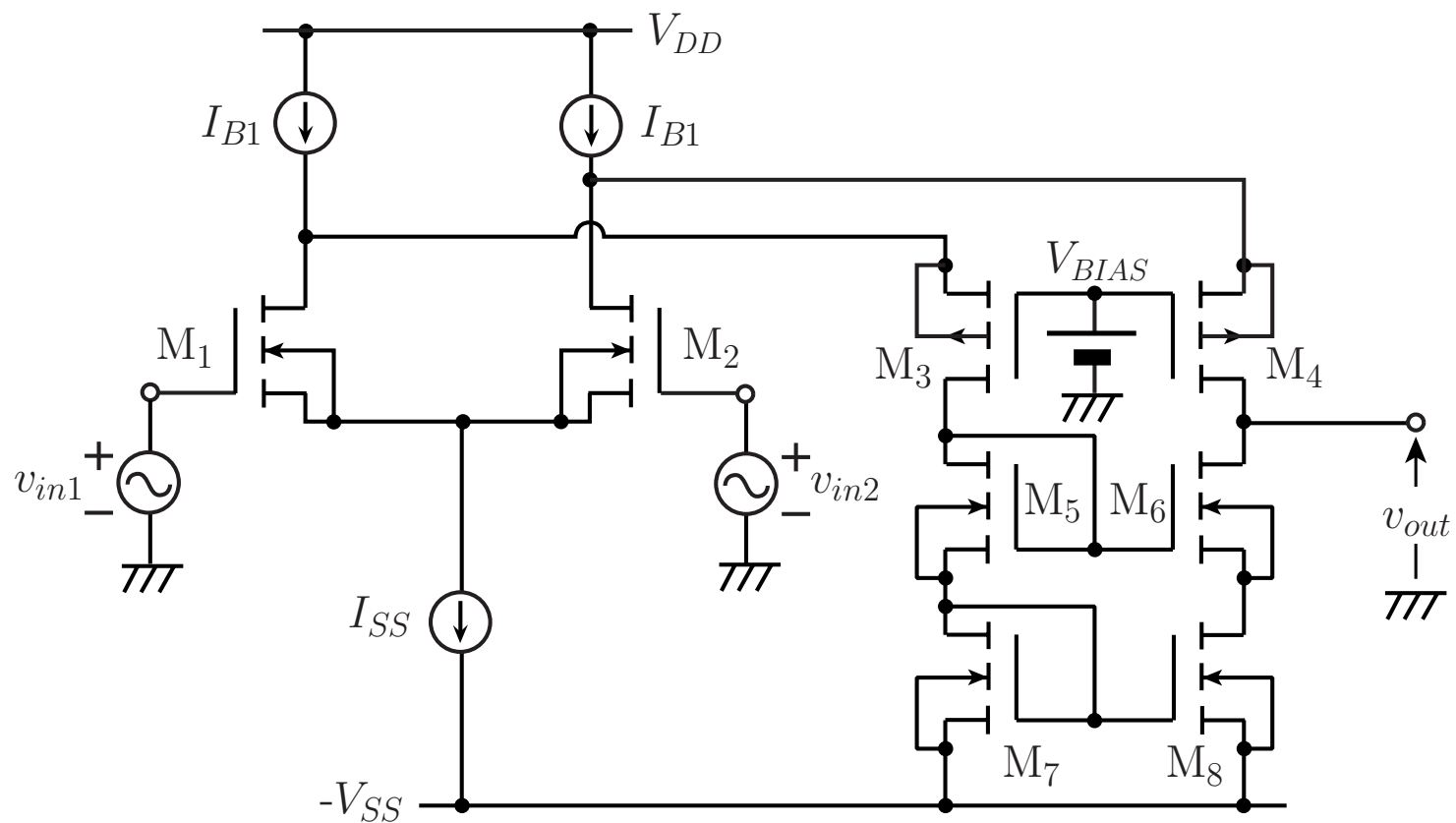
カスコード接続

出力抵抗の増加

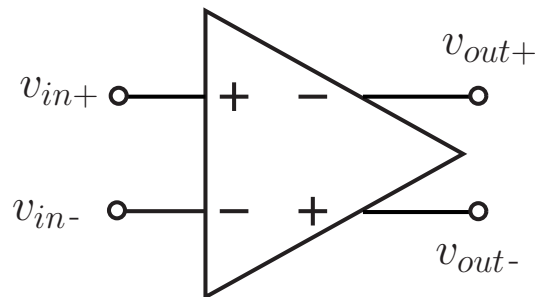
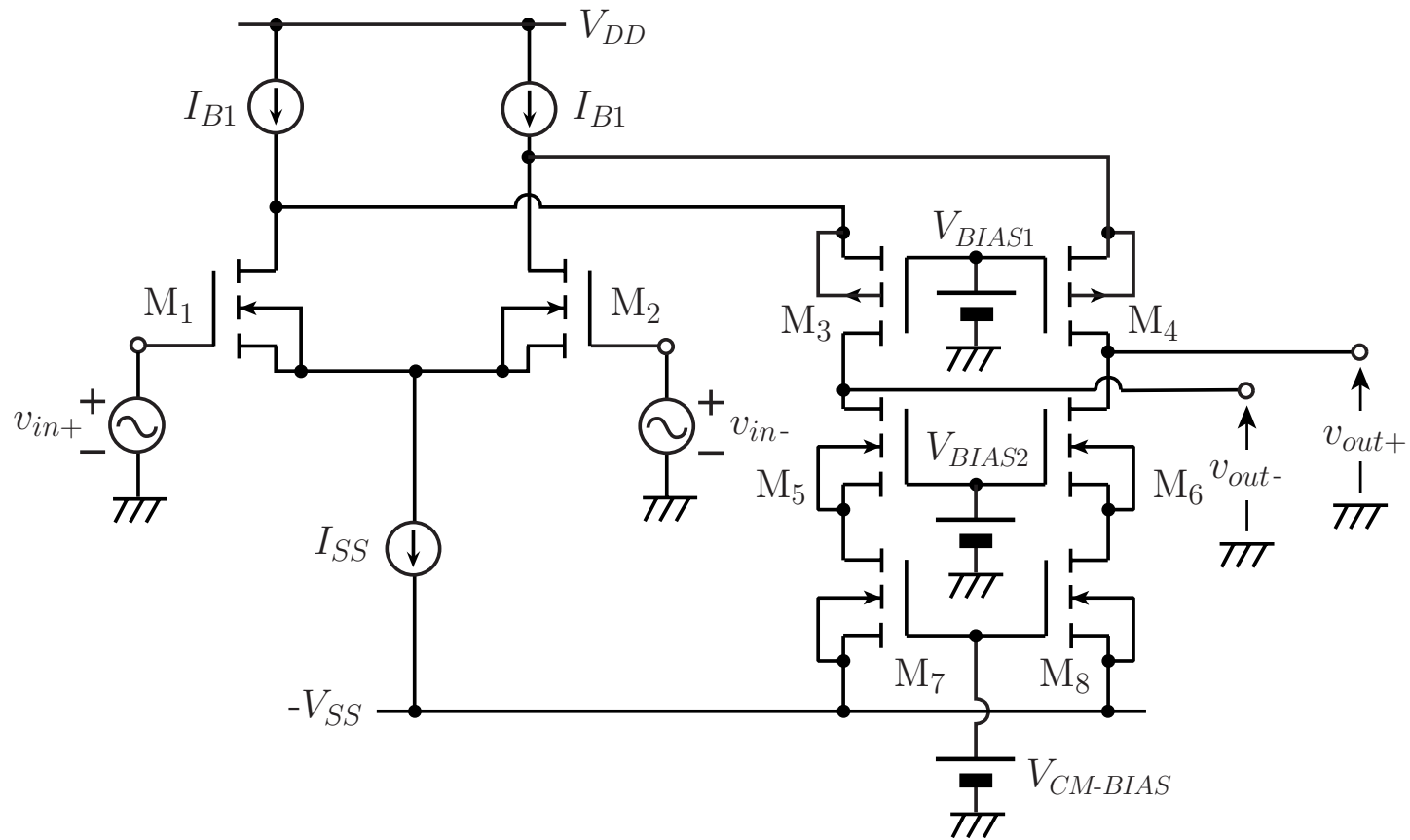
バイポーラトランジスタを用いたカスコード型演算増幅器



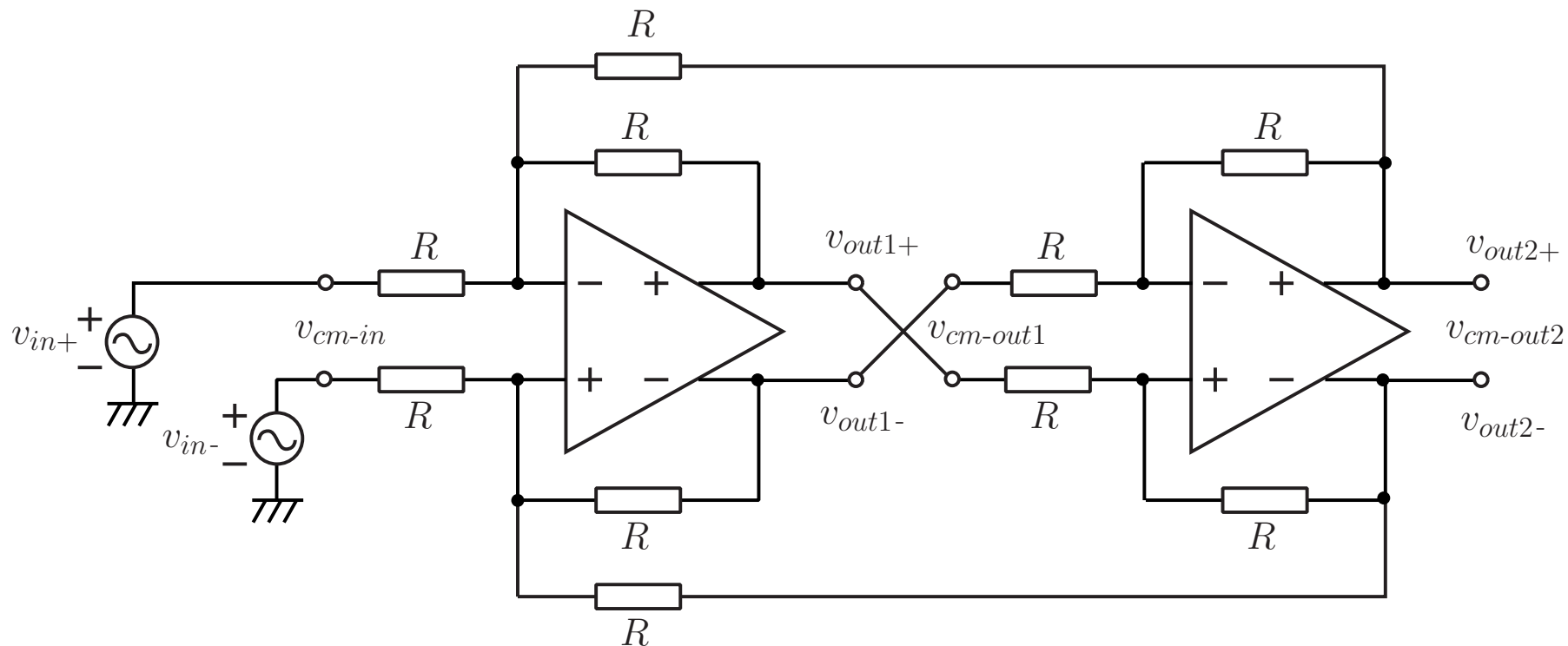
MOSトランジスタを用いたカスコード型演算増幅器



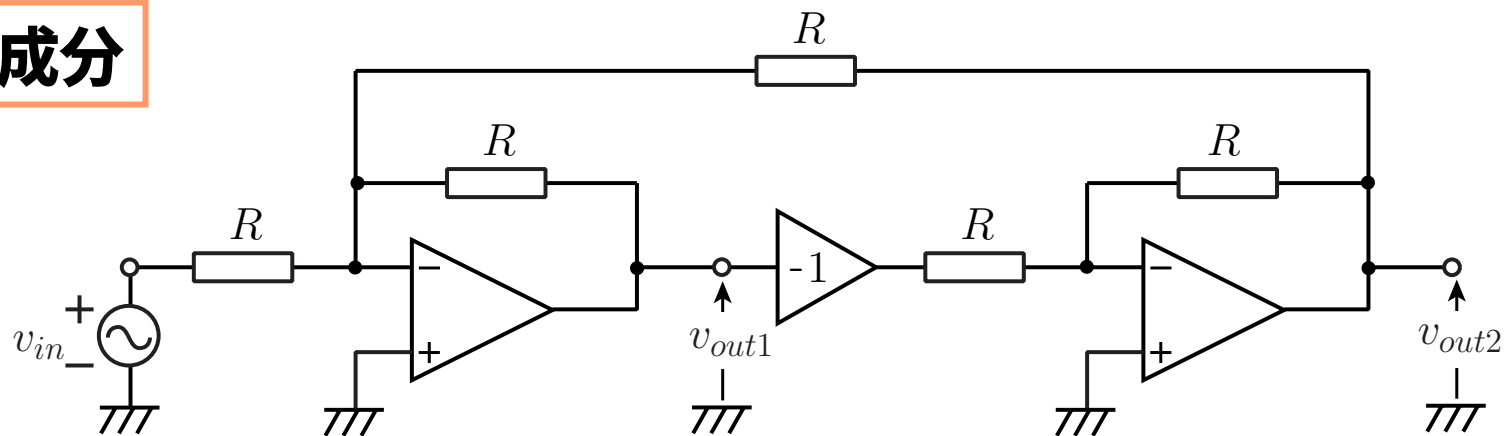
平衡型演算增幅器

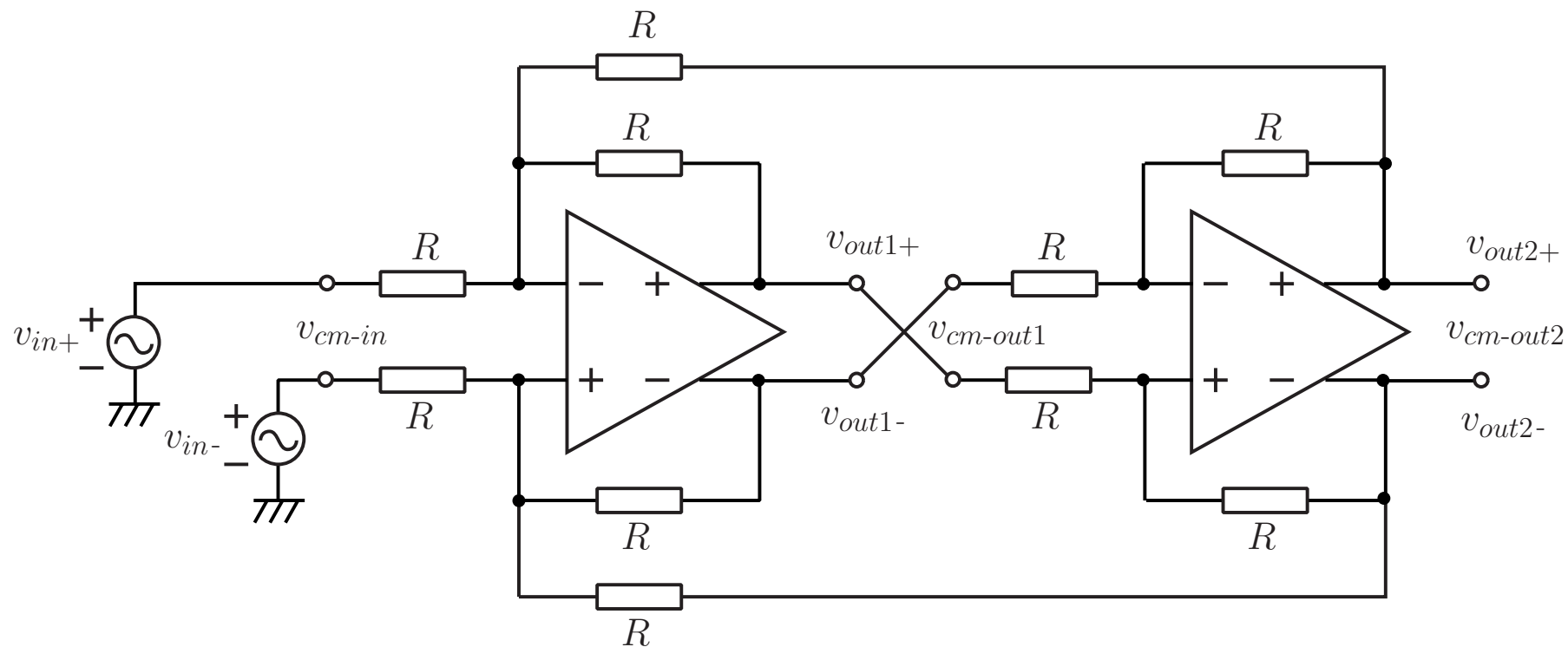


平衡型回路における同相帰還

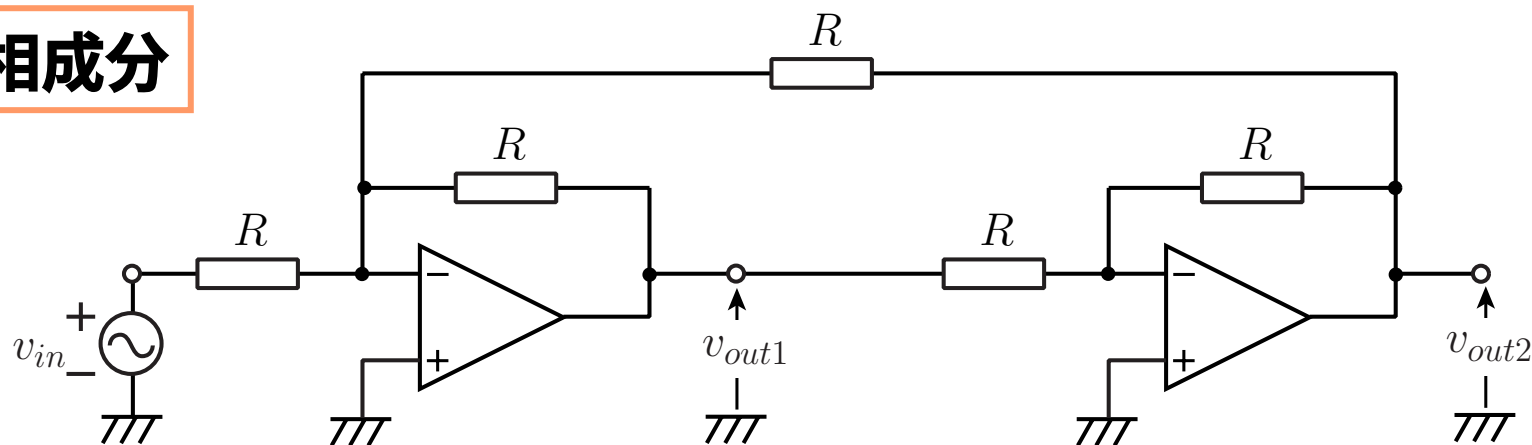


差動成分

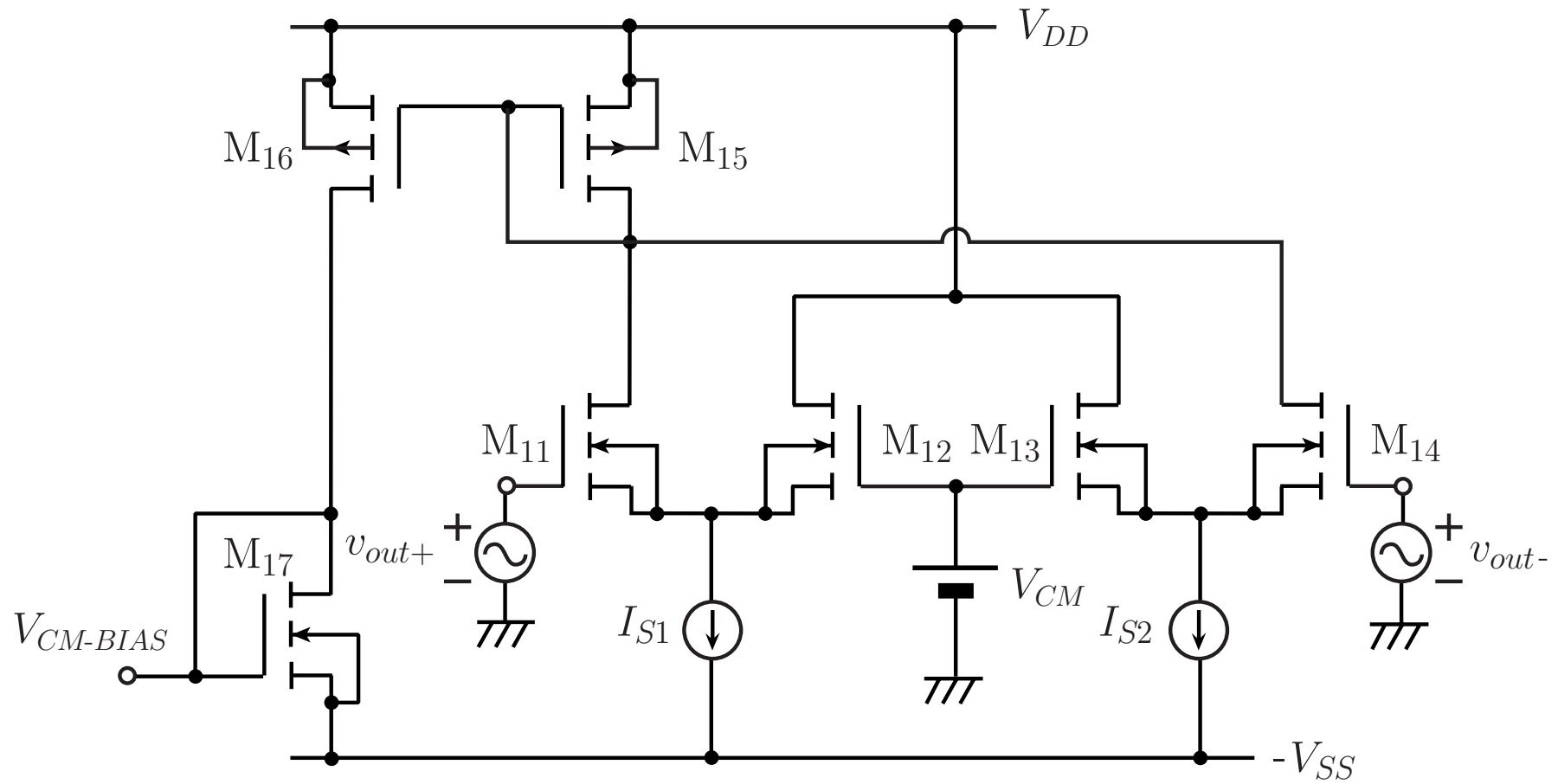




同相成分



バイアスの安定化



平衡型演算增幅器 (全回路)

