

11.Coupler and divider

11.1 Magic-T

11.2 Directional coupler

metallic hollow waveguide

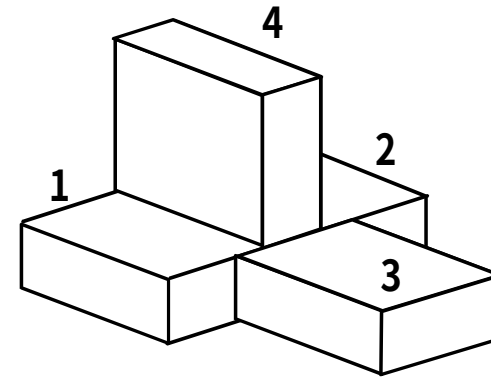
11.3 Design of hybrid in a strip line

11.4 Directional coupler composed of coupled dielectric waveguides

Magic-T

4 port reciprocal circuit:

$$\begin{bmatrix} S_{11} & S_{12} & S_{13} & S_{14} \\ S_{12} & S_{22} & S_{23} & S_{24} \\ S_{13} & S_{23} & S_{33} & S_{34} \\ S_{14} & S_{24} & S_{34} & S_{44} \end{bmatrix}$$

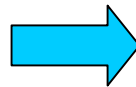


symmetry



$$\begin{bmatrix} S_{11} & S_{12} & S_{13} & S_{14} \\ S_{12} & \boxed{S_{11}} & \boxed{S_{13}} & S_{24} \\ S_{13} & \boxed{S_{13}} & S_{33} & S_{34} \\ S_{14} & S_{24} & S_{34} & S_{44} \end{bmatrix}$$

input from port 4: $S_{14} = -S_{24}$



$$\begin{bmatrix} S_{11} & S_{12} & S_{13} & S_{14} \\ S_{12} & S_{11} & S_{13} & \boxed{-S_{14}} \\ S_{13} & S_{13} & S_{33} & S_{34} \\ S_{14} & \boxed{-S_{14}} & S_{34} & S_{44} \end{bmatrix}$$

Magic-T

port 3 and 4 are isolated.

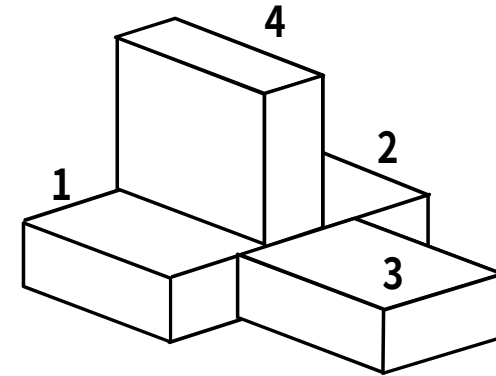
$$S_{34} = S_{43} = 0$$

port 3 and 4 are matched.

$$S_{33} = S_{44} = 0$$

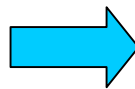


$$\begin{bmatrix} S_{11} & S_{12} & S_{13} & S_{14} \\ S_{12} & S_{11} & S_{13} & -S_{14} \\ S_{13} & S_{13} & \boxed{0} & \boxed{0} \\ S_{14} & -S_{14} & \boxed{0} & \boxed{0} \end{bmatrix}$$



loss-less:

$$\begin{cases} |S_{11}|^2 + |S_{12}|^2 + |S_{13}|^2 + |S_{14}|^2 = 1 \\ 2|S_{13}|^2 = 1 \\ 2|S_{14}|^2 = 1 \end{cases}$$



$$S_{13} = \frac{1}{\sqrt{2}} e^{j\varphi}$$

$$S_{14} = \frac{1}{\sqrt{2}} e^{j\theta}$$

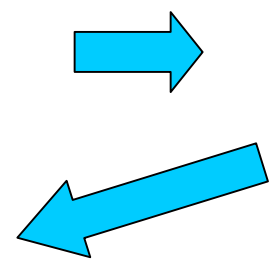
$$S_{11} = S_{12} = 0$$



$$\begin{bmatrix} 0 & 0 & \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} \\ 0 & 0 & \frac{1}{\sqrt{2}} & -\frac{1}{\sqrt{2}} \\ \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} & 0 & 0 \\ \frac{1}{\sqrt{2}} & -\frac{1}{\sqrt{2}} & 0 & 0 \end{bmatrix}$$

Directional coupler

reciprocity $\rightarrow$ symmetry of S
 matched at port 1 and 2
 port 1-2, port 3-4 are uncoupled.



$$\begin{bmatrix} 0 & 0 & S_{13} & S_{14} \\ 0 & 0 & S_{23} & S_{24} \\ S_{13} & S_{23} & S_{33} & 0 \\ S_{14} & S_{24} & 0 & S_{44} \end{bmatrix}$$

$$\left\{ \begin{array}{l} |S_{13}|^2 + |S_{14}|^2 = 1 \\ |S_{23}|^2 + |S_{24}|^2 = 1 \\ |S_{13}|^2 + |S_{23}|^2 + |S_{33}|^2 = 1 \\ |S_{14}|^2 + |S_{24}|^2 + |S_{44}|^2 = 1 \\ S_{13}S_{23}^* + S_{14}S_{24}^* = 0 \\ S_{13}S_{33}^* = 0 \\ S_{14}S_{44}^* = 0 \\ S_{23}S_{33}^* = 0 \\ S_{24}S_{44}^* = 0 \\ S_{13}S_{14}^* + S_{23}S_{24}^* = 0 \end{array} \right.$$

$|S_{13}|^2 + |S_{14}|^2 + |S_{23}|^2 + |S_{24}|^2 + |S_{33}|^2 + |S_{44}|^2 = 2$

$S_{33} = S_{44} = 0$

$|S_{13}|^2 + |S_{23}|^2 = 1$

$|S_{14}| = |S_{23}|$

$|S_{13}| = |S_{24}|$

Directional coupler

$$\begin{cases}
 |S_{13}|^2 + |S_{14}|^2 = 1 \\
 |S_{23}|^2 + |S_{24}|^2 = 1 \\
 |S_{13}|^2 + |S_{23}|^2 + |S_{33}|^2 = 1 \\
 |S_{14}|^2 + |S_{24}|^2 + |S_{44}|^2 = 1 \\
 S_{13}S_{23}^* + S_{14}S_{24}^* = 0 \\
 S_{13}S_{33}^* = 0 \\
 S_{14}S_{44}^* = 0 \\
 S_{23}S_{33}^* = 0 \\
 S_{24}S_{44}^* = 0 \\
 S_{13}S_{14}^* + S_{23}S_{24}^* = 0
 \end{cases}$$

$$|S_{13}| = |S_{24}|$$

$$S_{13} = S_{24} = \alpha$$

$$\begin{aligned}
 S_{14} &= j\beta \\
 S_{23} &= (-S_{14})^* = j\beta
 \end{aligned}$$

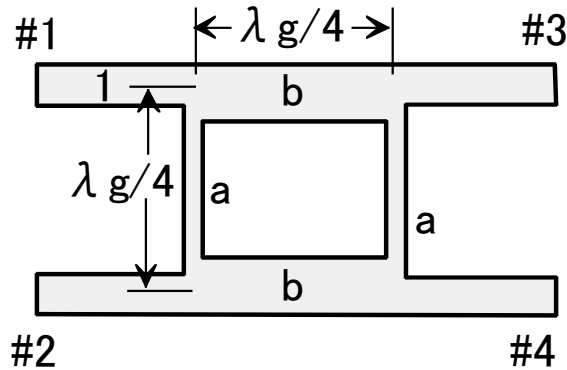
$$\begin{bmatrix}
 0 & 0 & S_{13} & S_{14} \\
 0 & 0 & S_{23} & S_{24} \\
 S_{13} & S_{23} & S_{33} & 0 \\
 S_{14} & S_{24} & 0 & S_{44}
 \end{bmatrix}$$



$$\begin{bmatrix}
 0 & 0 & \alpha & j\beta \\
 0 & 0 & j\beta & \alpha \\
 \alpha & j\beta & 0 & 0 \\
 j\beta & \alpha & 0 & 0
 \end{bmatrix}$$

$$\alpha = \beta = \frac{1}{\sqrt{2}} : 3\text{dB coupler}$$

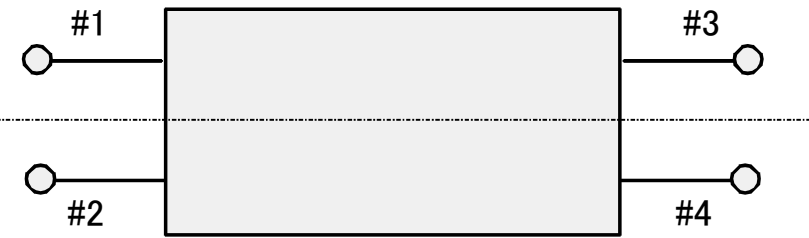
Design of a strip line directional coupler



even odd

$$\begin{aligned} &\frac{1}{\sqrt{2}} + \frac{1}{\sqrt{2}} \\ &\frac{1}{\sqrt{2}} + \left(-\frac{1}{\sqrt{2}}\right) \end{aligned}$$

uniaxial symmetry



$$\begin{bmatrix} b_1 \\ b_2 \\ b_3 \\ b_4 \end{bmatrix} = \begin{bmatrix} S_{11} & S_{21} & S_{31} & S_{41} \\ S_{21} & S_{11} & S_{41} & S_{31} \\ S_{31} & S_{41} & S_{33} & S_{43} \\ S_{41} & S_{31} & S_{43} & S_{33} \end{bmatrix} \begin{bmatrix} a_1 \\ a_2 \\ a_3 \\ a_4 \end{bmatrix}$$

even excitation

$$a_1 = a_2 = \frac{1}{\sqrt{2}} \quad a_3 = a_4 = 0$$

$$b_1 = b_2 = \frac{1}{\sqrt{2}} (S_{11} + S_{21}),$$

$$b_3 = b_4 = \frac{1}{\sqrt{2}} (S_{31} + S_{41})$$

$$\begin{aligned} \Gamma_e &= \frac{b_1}{a_1} = \frac{b_2}{a_2} = S_{11} + S_{21} \\ T_e &= \frac{b_3}{a_1} = \frac{b_4}{a_2} = S_{31} + S_{41} \end{aligned}$$

odd excitation

$$a_1 = -a_2 = \frac{1}{\sqrt{2}} \quad a_3 = a_4 = 0$$

$$b_1 = -b_2 = \frac{1}{\sqrt{2}} (S_{11} - S_{21}),$$

$$b_3 = -b_4 = \frac{1}{\sqrt{2}} (S_{31} - S_{41})$$

$$\begin{aligned} \Gamma_o &= \frac{b_1}{a_1} = \frac{b_2}{a_2} = S_{11} - S_{21} \\ T_o &= \frac{b_3}{a_1} = \frac{b_4}{a_2} = S_{31} - S_{41} \end{aligned}$$

uniaxial symmetric structure : S_{ij} and Γ , T

A uniaxially symmetric four-port circuit can be treated as two types of two port circuit.

$$S_{11} = \frac{1}{2}(\Gamma_e + \Gamma_o)$$

$$S_{21} = \frac{1}{2}(\Gamma_e - \Gamma_o)$$

$$S_{31} = \frac{1}{2}(T_e + T_o)$$

$$S_{41} = \frac{1}{2}(T_e - T_o)$$

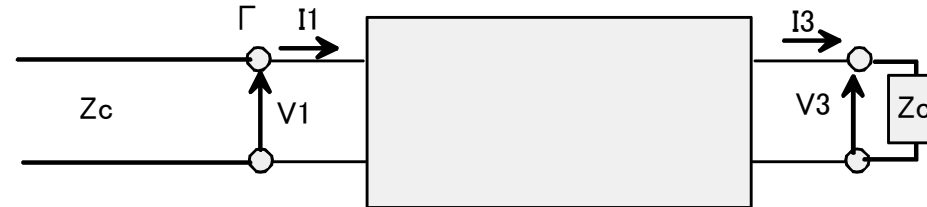
How to define Γ and T ?

$$\begin{pmatrix} V_1 \\ I_1 \end{pmatrix} = \begin{pmatrix} A & B \\ C & D \end{pmatrix} \begin{pmatrix} V_3 \\ I_3 \end{pmatrix}$$

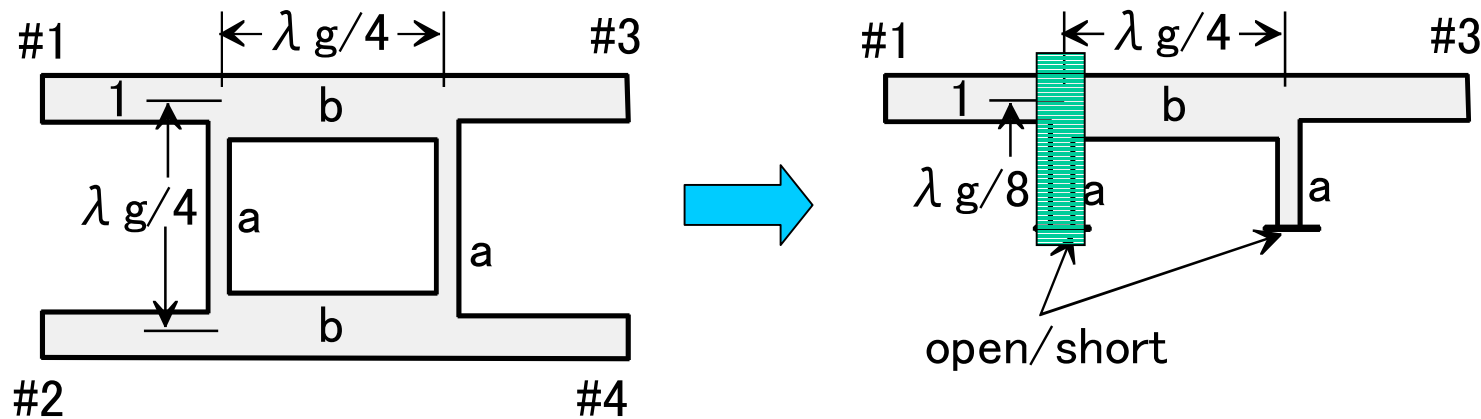
$$Z_1 = \frac{V_1}{I_1} = \frac{AV_3 + BI_3}{CV_3 + DI_3} = \frac{AZ_c + B}{CZ_c + D}$$

$$\Gamma = \frac{Z_1 - Z_c}{Z_1 + Z_c} = \frac{A + \frac{B}{Z_c} - CZ_c - D}{A + \frac{B}{Z_c} + CZ_c + D}$$

$$T = \frac{b_3}{a_1} = \frac{V_3 - Z_c(-I_3)}{V_1 + Z_c I_1} = \frac{2}{A + \frac{B}{Z_c} + CZ_c + D}$$



Design of a strip line directional coupler : F-matrix



1) open (or short) stub:

$$V_1 = V_2$$

$$I_1 = \frac{V_2}{z} + I_2$$

$$F = \begin{pmatrix} 1 & 0 \\ \frac{1}{z} & 1 \end{pmatrix}$$

$$\text{open} : z = -jz_c = -j \frac{1}{a} \quad (\because \beta l = \frac{\pi}{4})$$

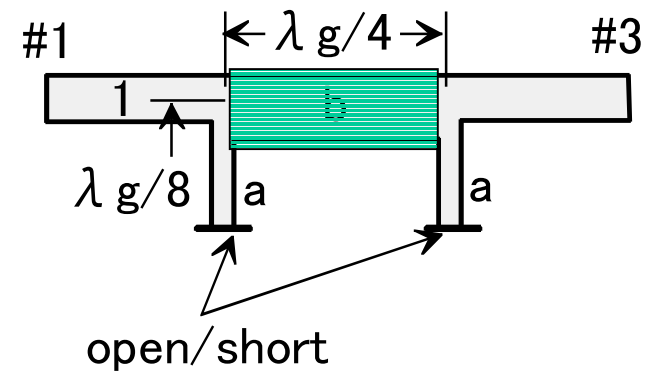
$$\text{short} : z = jz_c = j \frac{1}{a}$$

Design of a strip line directional coupler : F-matrix

2) transmission line of length $\lambda_g/4$ ($\beta l = \frac{\pi}{2}$)

$$\begin{pmatrix} V_1 \\ I_1 \end{pmatrix} = \begin{pmatrix} \cos \beta l & j \frac{1}{b} \sin \beta l \\ j b \sin \beta l & \cos \beta l \end{pmatrix} \begin{pmatrix} V_2 \\ I_2 \end{pmatrix}$$

$$F = \begin{pmatrix} 0 & j \frac{1}{b} \\ j b & 0 \end{pmatrix}$$



Γ and T for eigen excitation

even excitation:

$$[F_e] = \begin{pmatrix} 1 & 0 \\ ja & 1 \end{pmatrix} \begin{pmatrix} 0 & j\frac{1}{b} \\ jb & 0 \end{pmatrix} \begin{pmatrix} 1 & 0 \\ ja & 1 \end{pmatrix} = \begin{pmatrix} -\frac{a}{b} & j\frac{1}{b} \\ j\left(b - \frac{a^2}{b}\right) & -\frac{a}{b} \end{pmatrix}$$

$$\Gamma_e = \frac{j\left(\frac{1}{b} - b + \frac{a^2}{b}\right)}{-\frac{2a}{b} + j\left(\frac{1}{b} + b - \frac{a^2}{b}\right)}, \quad T_e = \frac{2}{-\frac{2a}{b} + j\left(\frac{1}{b} + b - \frac{a^2}{b}\right)}$$

odd excitation:

$$[F_o] = \begin{pmatrix} 1 & 0 \\ -ja & 1 \end{pmatrix} \begin{pmatrix} 0 & j\frac{1}{b} \\ jb & 0 \end{pmatrix} \begin{pmatrix} 1 & 0 \\ -ja & 1 \end{pmatrix} = \begin{pmatrix} \frac{a}{b} & j\frac{1}{b} \\ j\left(b - \frac{a^2}{b}\right) & \frac{a}{b} \end{pmatrix}$$

$$\Gamma_o = \frac{j\left(\frac{1}{b} - b + \frac{a^2}{b}\right)}{\frac{2a}{b} + j\left(\frac{1}{b} + b - \frac{a^2}{b}\right)}, \quad T_o = \frac{2}{\frac{2a}{b} + j\left(\frac{1}{b} + b - \frac{a^2}{b}\right)}$$

3dB condition

$$S_{11} = \frac{1}{2}(\Gamma_e + \Gamma_o) = 0, \quad S_{21} = \frac{1}{2}(\Gamma_e - \Gamma_o) = 0$$



$$\Gamma_e = \Gamma_o = 0$$

$$\therefore 1 + a^2 = b^2$$

$$T_e = \frac{2}{-\frac{2a}{b} + j\left(\frac{1}{b} + b - \frac{a^2}{b}\right)} \quad T_o = \frac{2}{\frac{2a}{b} + j\left(\frac{1}{b} + b - \frac{a^2}{b}\right)}$$

$$S_{31} = \frac{1}{2}(T_e + T_o), \quad S_{41} = \frac{1}{2}(T_e - T_o)$$

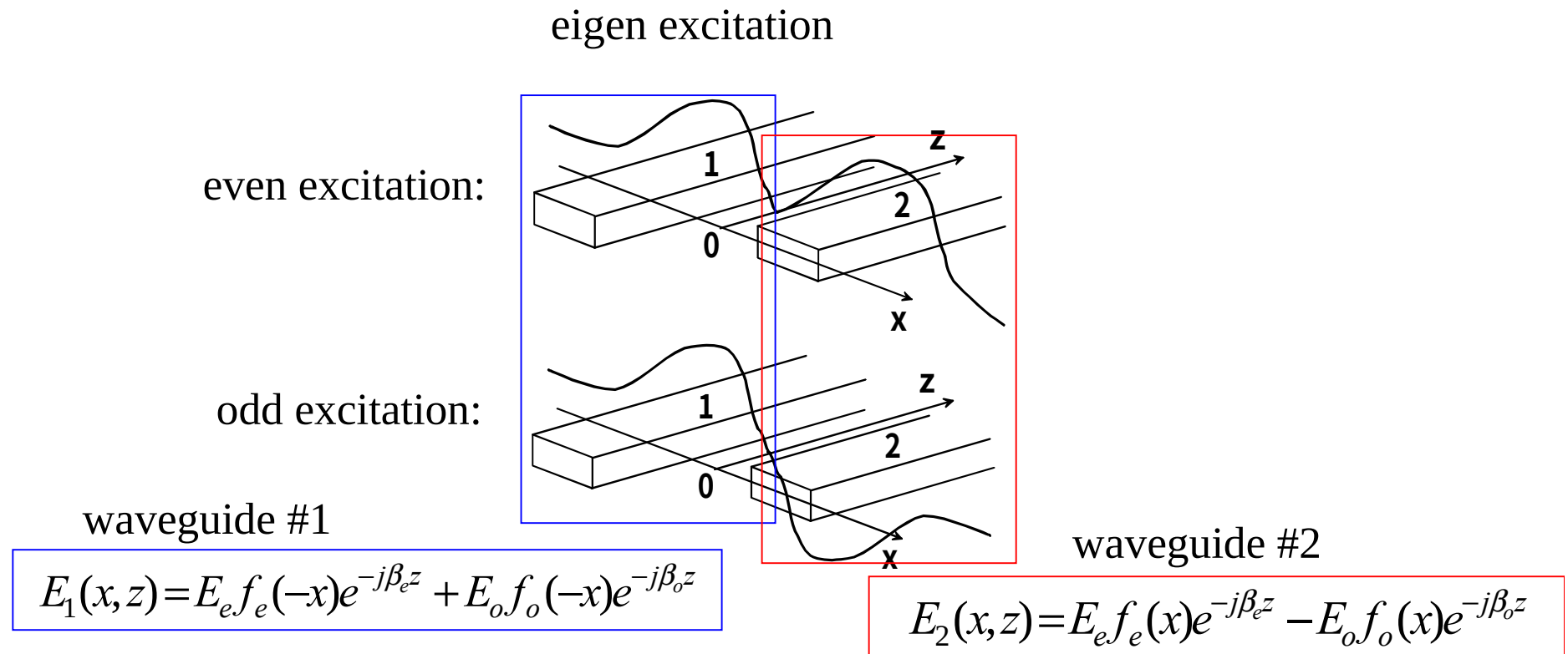


$$S_{31} = -j\frac{1}{b}, \quad S_{41} = -\frac{a}{b}$$

$$\text{3-dB} \quad |S_{31}| = |S_{41}| = \frac{1}{\sqrt{2}} \quad \longrightarrow \quad a = 1, \quad b = \sqrt{2}$$

$$\begin{bmatrix} 0 & 0 & j\frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} \\ 0 & 0 & \frac{1}{\sqrt{2}} & j\frac{1}{\sqrt{2}} \\ j\frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} & 0 & 0 \\ \frac{1}{\sqrt{2}} & j\frac{1}{\sqrt{2}} & 0 & 0 \end{bmatrix}$$

Directional coupler : coupled dielectric waveguide



$$f_e(x) \approx f_o(x) \approx f(x) = f(-x)$$

Coupled dielectric waveguide : input from port 1

$$\begin{pmatrix} E_1(x, z) \\ E_2(x, z) \end{pmatrix} = \begin{pmatrix} T_{11} & T_{12} \\ T_{21} & T_{22} \end{pmatrix} \begin{pmatrix} E_1(x, 0) \\ E_2(x, 0) \end{pmatrix}$$

input from port 1

$$\begin{pmatrix} E_1(x, z) \\ E_2(x, z) \end{pmatrix} = \begin{pmatrix} T_{11} & T_{12} \\ T_{21} & T_{22} \end{pmatrix} \begin{pmatrix} f(-x) \\ 0 \end{pmatrix}$$

$$f_e(x) \approx f_o(x) \approx f(x) = f(-x) \quad E_e = E_o = 1/2$$

$$\begin{aligned} E_1(x, z) &= T_{11}f(-x) = E_e f_e(-x)e^{-j\beta_e z} + E_o f_o(-x)e^{-j\beta_o z} \\ &= \frac{f(-x)}{2} (e^{-j\beta_e z} + e^{-j\beta_o z}) = \cos\left(\frac{\beta_e - \beta_o}{2} z\right) e^{-j\frac{\beta_e + \beta_o}{2} z} f(-x) \quad \therefore T_{11} = \cos\left(\frac{\beta_e - \beta_o}{2} z\right) e^{-j\frac{\beta_e + \beta_o}{2} z} \end{aligned}$$

$$\begin{aligned} E_2(x, z) &= T_{21}f(-x) = E_e f_e(x)e^{-j\beta_e z} - E_o f_o(x)e^{-j\beta_o z} \\ &= -j \sin\left(\frac{\beta_e - \beta_o}{2} z\right) e^{-j\frac{\beta_e + \beta_o}{2} z} f(-x) \quad \therefore T_{21} = -j \sin\left(\frac{\beta_e - \beta_o}{2} z\right) e^{-j\frac{\beta_e + \beta_o}{2} z} \end{aligned}$$

Coupled dielectric waveguide : input from port 2

input from port 2

$$\begin{pmatrix} E_1(x, z) \\ E_2(x, z) \end{pmatrix} = \begin{pmatrix} T_{11} & T_{12} \\ T_{21} & T_{22} \end{pmatrix} \begin{pmatrix} 0 \\ f(x) \end{pmatrix} \quad E_e = -E_o = 1/2$$

$$\begin{aligned} E_1(x, z) &= T_{12}f(x) = E_e f_e(-x)e^{-j\beta_e z} + E_o f_o(-x)e^{-j\beta_o z} \\ &= \frac{f(-x)}{2} (e^{-j\beta_e z} - e^{-j\beta_o z}) = -j \sin\left(\frac{\beta_e - \beta_o}{2} z\right) e^{-j\frac{\beta_e + \beta_o}{2} z} f(x) \quad \therefore T_{12} = -j \sin\left(\frac{\beta_e - \beta_o}{2} z\right) e^{-j\frac{\beta_e + \beta_o}{2} z} \end{aligned}$$

$$\begin{aligned} E_2(x, z) &= T_{22}f(x) = E_e f_e(x)e^{-j\beta_e z} - E_o f_o(x)e^{-j\beta_o z} \\ &= \cos\left(\frac{\beta_e - \beta_o}{2} z\right) e^{-j\frac{\beta_e + \beta_o}{2} z} f(x) \quad \therefore T_{22} = \cos\left(\frac{\beta_e - \beta_o}{2} z\right) e^{-j\frac{\beta_e + \beta_o}{2} z} \end{aligned}$$

$$\begin{pmatrix} T_{11} & T_{21} \\ T_{12} & T_{22} \end{pmatrix} = \begin{pmatrix} \cos\left(\frac{\beta_e - \beta_o}{2} z\right) & -j \sin\left(\frac{\beta_e - \beta_o}{2} z\right) \\ -j \sin\left(\frac{\beta_e - \beta_o}{2} z\right) & \cos\left(\frac{\beta_e - \beta_o}{2} z\right) \end{pmatrix} e^{-j\frac{\beta_e + \beta_o}{2} z}$$

Directional coupler : coupled dielectric waveguide

coupling coefficient : $\kappa = \frac{\beta_e - \beta_o}{2}$

$$[T] = \begin{pmatrix} \cos \kappa z & -j \sin \kappa z \\ -j \sin \kappa z & \cos \kappa z \end{pmatrix} e^{-j \frac{\beta_e + \beta_o}{2} z}$$

100% coupling : $\kappa z = \pi / 2$

$$[T] = \begin{pmatrix} 0 & -j \\ -j & 0 \end{pmatrix} e^{-j \frac{\beta_e + \beta_o}{2} z}$$

50% coupling : $\kappa z = \pi / 4$

$$[T] = \begin{pmatrix} \frac{1}{\sqrt{2}} & -j \frac{1}{\sqrt{2}} \\ -j \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} \end{pmatrix} e^{-j \frac{\beta_e + \beta_o}{2} z}$$