

数値解析への入り口

Entrance to numerical analysis

For vibration simulation of complicated structures, numerical methods are used.

0.Preparation : vibration in a string

1.Energy methods

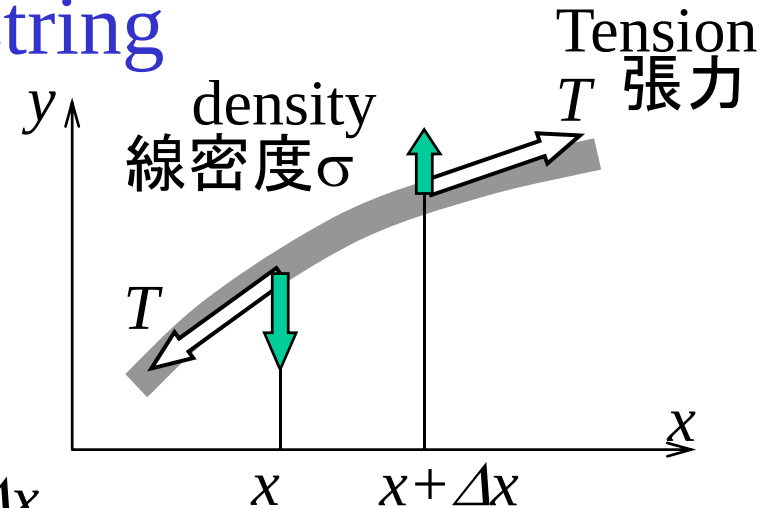
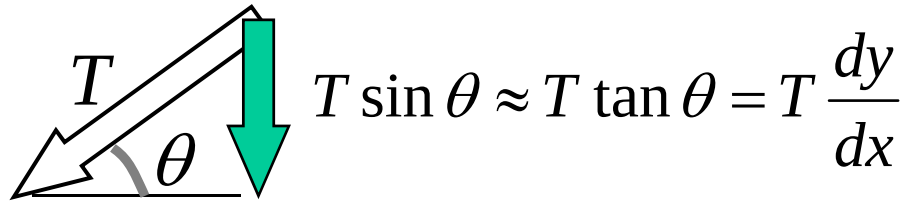
- 1) Rayleigh method

- 2) Ritz method

2.Discrete methods

弦の振動 1 Vibration of a string

Vertical components of tension at $x=x$



Vertical components of tension at $x=x + \Delta x$

$$\left. \frac{dy}{dx} \right|_{x=x+\Delta x} = \frac{dy}{dx} + \frac{d^2 y}{dx^2} \Delta x \quad \text{より} \quad T \frac{dy}{dx} + T \frac{d^2 y}{dx^2} \Delta x$$

From the equilibrium between the vertical component of the tension and the inertial force acting on the small part:

$$T \frac{d^2 y}{dx^2} = \sigma \frac{d^2 y}{dt^2}$$

Wave equation for vibration of a string

弦の振動2 Vibration of a string

弦の波動方程式 $\frac{d^2 y}{dx^2} = \frac{1}{c^2} \frac{d^2 y}{dt^2}$
Wave equation

弦振動の伝搬速度 $c = \sqrt{\frac{T}{\sigma}}$ $\left\{ \begin{array}{l} T, \text{ 張力 [N]} \\ \sigma, \text{ 線密度 [kg/m]} \end{array} \right.$
Propagation speed

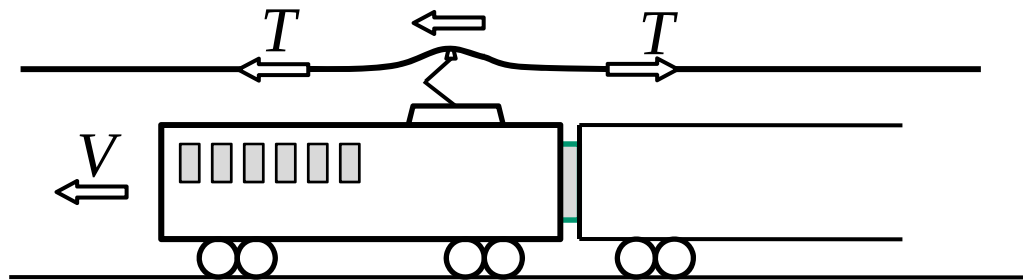
弦の最大許容応力を $P_{\max}$ として、最大伝搬速度は $c_{\max} = \sqrt{\frac{P_{\max}}{\rho}}$

Assuming the maximum stress without failure $P_{\max}$, the maximum propagation speed of $c_{\max}$ can be defined.

Maximum speed of electric train

Max. safety stress in the feeding line, $P_{\max}$

Speed of the train should be smaller than the wave propagation to keep stable contact between the feeding line and the pantograph.



$$V < c_{\max} = \sqrt{\frac{P_{\max}}{\rho}}$$

Strength of materials

Duralumin A2017 = 500 MPa, S-duralumin A2024 = 323 MPa

SS-duralumin A7075 = 505 MPa, Steel S45C = 727 MPa

Stainless steel SUS304 = 205 MPa, Ti = 800 MPa

Max speed of the train: SUS304 → 580 km/h; A7075 → 1500 km/h

Energy method 1

両端固定の弦



厳密解 $\omega_1^2 = \frac{2.46740}{l^2} \left(\frac{T}{\sigma} \right)$
Analytic solution

$$\omega_2^2 = \frac{22.207}{l^2} \left(\frac{T}{\sigma} \right)$$

張力 T , 線密度 σ , 長さ $2l$

Rayleigh法

$$T_{\max} = U_{\max} \quad \left\{ \begin{array}{l} T: \text{運動エネルギー Kinetic energy} \\ U: \text{ポテンシャルエネルギー Potential energy} \end{array} \right.$$

変位分布を仮定する。例えば、 $y = a(l^2 - x^2)$

Assume a displacement function:

$$\left. \begin{array}{l} T_{\max} = \int_{-l}^l \frac{1}{2} \rho \left(\frac{dy}{dt} \right)^2 dx = \int_{-l}^l \frac{1}{2} \rho \omega^2 y^2 dx \\ U_{\max} = \int_{-l}^l \frac{1}{2} T \left(\frac{dy}{dx} \right)^2 dx \end{array} \right\} \longrightarrow \omega_1^2 = \frac{2.5}{l^2} \left(\frac{T}{\sigma} \right)$$

誤差 +1.3%

Energy method 2:

Ritz法 $L = T_{\max} - U_{\max}$ を最小にする Minimize L

Assume the displacement as below:

変位分布を $y = a_1\varphi_1(x) + a_2\varphi_2(x) + \cdots + a_i\varphi_i(x) + \cdots$

として、 $\frac{\partial L}{\partial a_i} = 0$ より a_i を定める。

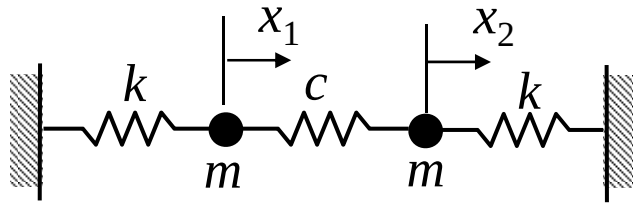
ここでは、例えば、 $y = a_1(l^2 - x^2) + a_2x^2(l^2 - x^2)$

境界条件を満たす関数形の線形結合

$$\begin{aligned} \longrightarrow \left\{ \begin{array}{ll} \omega_1^2 = \frac{2.46744}{l^2} \left(\frac{T}{\sigma} \right) & \text{誤差 } +0.0016\% \\ \omega_2^2 = \frac{25.6}{l^2} \left(\frac{T}{\sigma} \right) & \text{誤差 } +15\% \end{array} \right. \end{aligned}$$

Discrete method

Example: deg. of freedom = 2



$$\begin{pmatrix} x_1 \\ x_2 \end{pmatrix} = \mathbf{x} \quad \begin{array}{l} \text{変位ベクトル} \\ \text{Displacement vector} \end{array}$$

$$\begin{pmatrix} m & 0 \\ 0 & m \end{pmatrix} = \mathbf{M} \quad \begin{array}{l} \text{質量マトリックス} \\ \text{Mass matrix} \end{array}$$

$$\begin{pmatrix} k+c & -c \\ -c & k+c \end{pmatrix} = \mathbf{k} \quad \begin{array}{l} \text{弾性マトリックス} \\ \text{Elastic matrix} \end{array}$$

左側の質点に関する運動方程式

$$m \frac{d^2 x_1}{dt^2} = -kx_1 + c(x_2 - x_1)$$

右側の質点に関する運動方程式

$$m \frac{d^2 x_2}{dt^2} = -kx_2 - c(x_2 - x_1)$$

調和振動を考える＋行列表示

Harmonic case, matrix expression

$$-\omega^2 \begin{pmatrix} m & 0 \\ 0 & m \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \end{pmatrix} = - \begin{pmatrix} k+c & -c \\ -c & k+c \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \end{pmatrix}$$

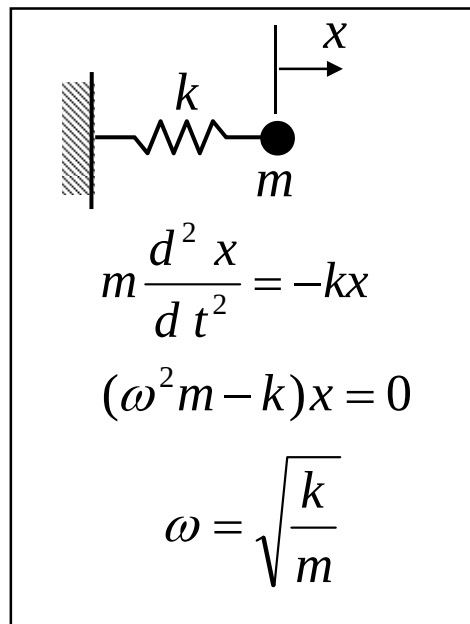
$$(\omega^2 \mathbf{M} - \mathbf{k}) \mathbf{x} = 0$$

共振周波数の式 $|\omega^2 \mathbf{M} - \mathbf{k}| = 0$

Frequency equation

Discrete method

単振り子との比較



$(\omega^2 \mathbf{M} - \mathbf{k})\mathbf{x} = 0$ 共振周波数の式

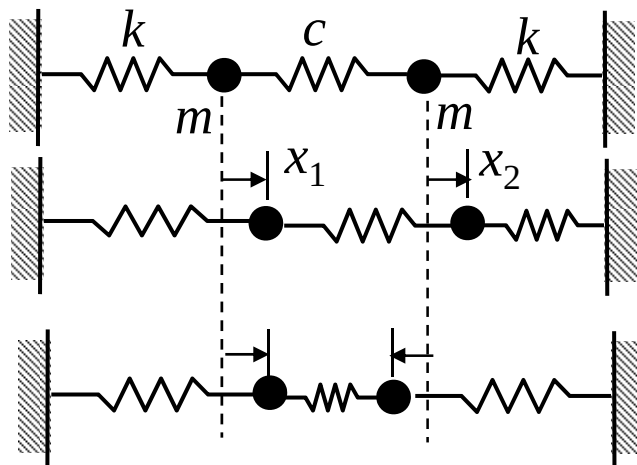
$$|\omega^2 \mathbf{M} - \mathbf{k}| = 0$$

$$\begin{vmatrix} \omega^2 m - (k + c) & -c \\ -c & \omega^2 m - (k + c) \end{vmatrix} = 0$$

$$(\omega^2 m - k)\{\omega^2 m - (k + 2c)\} = 0$$

$$\omega = \sqrt{\frac{k}{m}}, \quad \sqrt{\frac{k + 2c}{m}} \quad \text{共振周波数(固有値)}$$

Eigen values = resonance frequencies



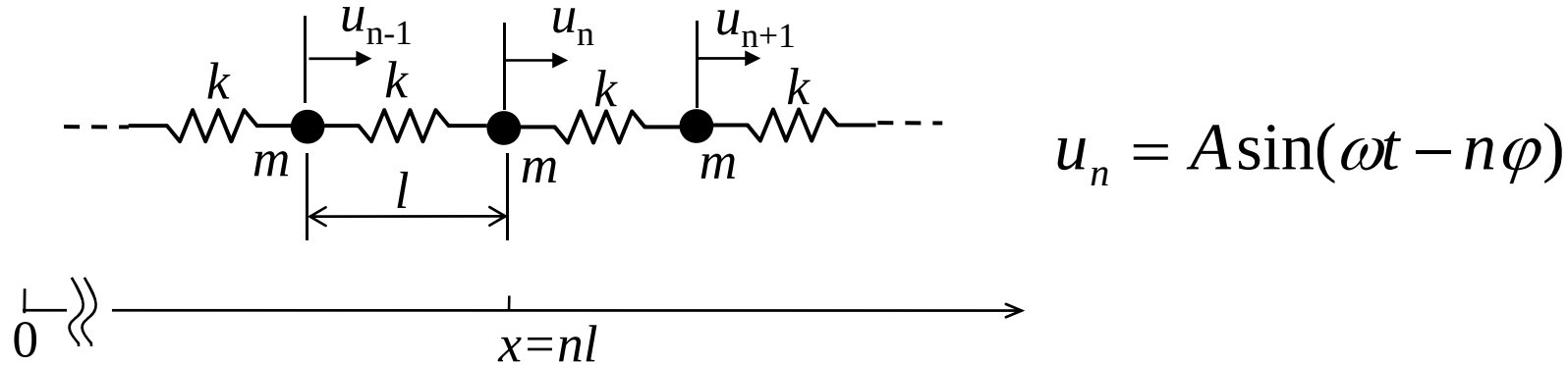
固有ベクトル = 振動モード

Eigen vector = vibration mode

$x_1 = x_2$ Lower mode

$x_1 = -x_2$ Higher mode

Sound speed in the discrete method (1/2)



Wave equation for the n-th mass

$$m \frac{d^2 u_n}{dt^2} = -k(u_n - u_{n-1}) + k(u_{n+1} - u_n)$$

$$m \frac{d^2 u_n}{dt^2} = -k \{ \sin(\omega t - n\varphi) - \sin(\omega t - n\varphi + \varphi) \} + k \{ \sin(\omega t - n\varphi - \varphi) - \sin(\omega t - n\varphi) \}$$

$$= -2kA \left\{ \cos\left(\omega t - n\varphi + \frac{\varphi}{2}\right) - \cos\left(\omega t - n\varphi - \frac{\varphi}{2}\right) \right\} \sin \frac{-\varphi}{2}$$

$$= -2kA \left\{ -2 \sin(\omega t - n\varphi) \sin \frac{-\varphi}{2} \right\} \sin \frac{-\varphi}{2}$$

$$= -4kA \sin(\omega t - n\varphi) \sin^2 \frac{\varphi}{2}$$

$$m \frac{d^2 u_n}{dt^2} = -\omega^2 A \sin(\omega t - n\varphi)$$

Sound speed in the discrete method (2/2)

$$\begin{cases} \omega_0 = \sqrt{k/m} \\ \omega \ll \omega_0 \end{cases} \quad \rightarrow \quad \frac{\omega}{\omega_0} = 2 \sin \frac{\varphi}{2} \approx \varphi$$

$$\frac{\varphi}{2\pi} = \frac{l}{\lambda}$$

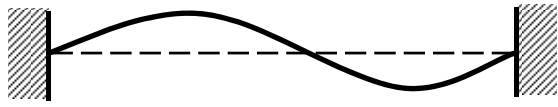
$$c = f\lambda = \frac{\omega}{2\pi} \lambda = \frac{\omega_0 \varphi}{2\pi} \lambda = \omega_0 l = l \sqrt{\frac{k}{m}} = \sqrt{\frac{kl}{m/l}}$$

$$c = \sqrt{\frac{kl/S}{m/lS}}$$

Elastic constant

Density

Question:



$$\omega_2^2 = \frac{22.207}{l^2} \left(\frac{T}{\sigma} \right) \quad \text{Analytic solution}$$

張力 T , 線密度 σ , 長さ $2l$

Assuming the displacement function as below, find the second resonance frequency using the Rayleigh method.

Displacement function: $y = ax(l^2 - x^2)$

$$T_{\max} = U_{\max}$$

$$\left. \begin{aligned} T_{\max} &= \int_{-l}^l \frac{1}{2} \rho \left(\frac{dy}{dt} \right)^2 dx = \int_{-l}^l \frac{1}{2} \rho \omega^2 y^2 dx \\ U_{\max} &= \int_{-l}^l \frac{1}{2} T \left(\frac{dy}{dx} \right)^2 dx \end{aligned} \right\} \longrightarrow \omega_2^2 ?$$