4. Fundamental Concepts of Fracture Mechanics

1.Introduction

During World War II

5000 ships built

over 1000 ships: cracks by 1946

200 ships: serious damage

9 T-2 tankers
7 Liberty ships

$\}$ broken in two

2

What is Fracture Mechanics?

Strength of Materials

Yield $\sigma = \sigma_y$

Failure $\sigma = \sigma_B$

Fatigue $S - N$ *Diagram, Fatigue Limit*

Fracture Mechanics

Failure $K = K_C$

Stress Intensity Factor K

Fracture Toughness K_C

Fatigue $\frac{da}{dN} = C\left((\Delta K)^m - (\Delta K_{th})^m\right)K_C$

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Fracture Mechanics is

Mechanics of Members with Cracks

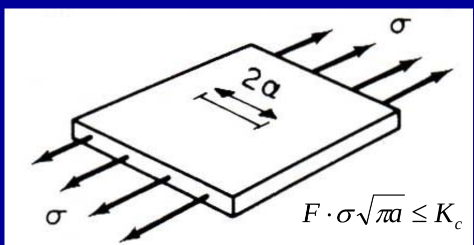
Stress Intensity Factor, K

Stress, σ

Crack Length, a

Fracture Toughness, Kc

Material Property



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Primary Factors controlling Brittle Fracture : 1

- 1) Material toughness (Kc, KIc, $K_{Id}=C\sigma\sqrt{a}$)
  - the ability to carry load or deform plastically in the presence of notch
  - for slow loading and linear -elastic behavior.
    - K_c :under conditions of plane stress
    - K_{Ic} :plane strain
  - impact or dynamic loading
    - K_{Id} : under condition of maximum constraint (plane strain)
  - For elastic-plastic behavior
    - R-curve resistance, J_{Ic}, and CTOD

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Primary Factors controlling Brittle Fracture : 2

- 2) Crack size (a)
  - Brittle ftacture initiate from discontinuities varying from small cracks within a weld ark strike (case in a T-2 tanker) to much larger fatigue cracks.
- 3) Stress level (σ): Tensile stress are necessary for brittle failure to occur.
- Brittle failure can occur without all three factors being present if the other factors are sufficiently severe.
- Other factors such as temperature, loading rate, stress concentration, residual stress, and so on will affect the three primary factors

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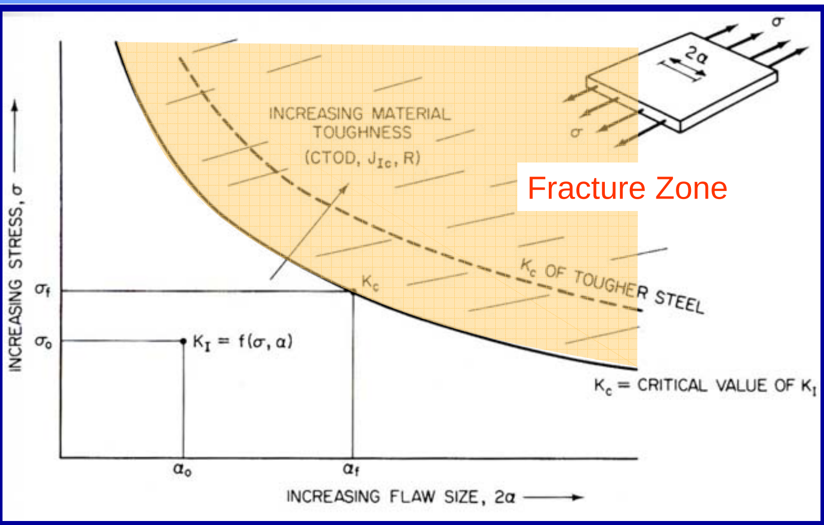
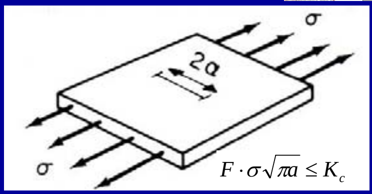
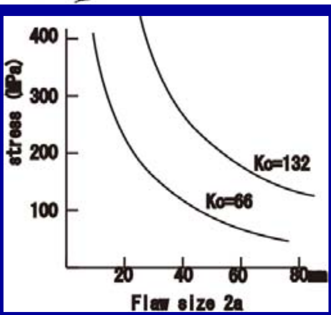
Fundamental Concepts of Fracture Mechanics



Relationship among a stress condition, a crack size and fracture toughness

Example





Consider a through thickness crack in a wide plate,

design stress is 38MPa ,310MPa

$K_I = \sigma\sqrt{\pi a}$ $K_c = 66{,}132 MPa\sqrt{m}$

what is the tolerable flaw size?

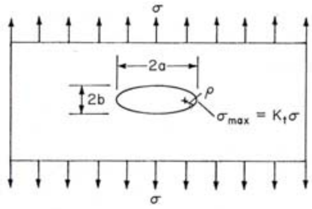
If residual stresses due to welding present so that the total stress is 552MPa at the crack.

	Kc=66	Kc=132
σ =138 MPa	2a=145mm	291
σ =310	27.9	57.7
σ =552	4.6	18.2

2.Meaning of Stress Analysis of Members with Notches

Types of Discontinuities

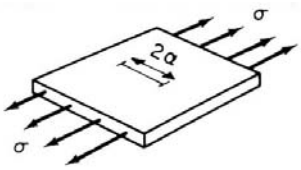
Notches



Imperfections

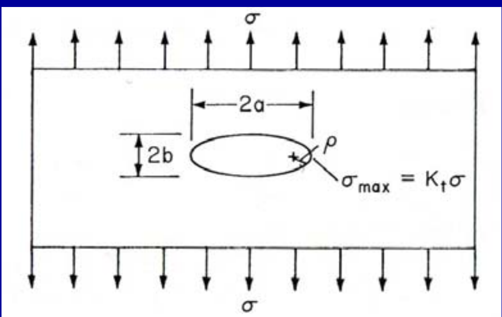
Sharp Tip

Cracks



Stress Concentration Factor :Kt

Kt For An Elliptical Hole



$$K_T = \frac{\sigma_{\max}}{\sigma} = 1 + \frac{2a}{b}$$

$$\rho = \frac{b^2}{a}$$

$$\sigma_{\max} \cong 2\sigma\sqrt{\frac{a}{\rho}} \quad (\rho << a)$$

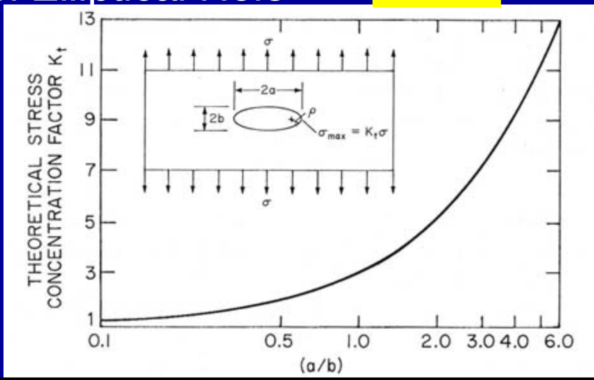
$$\sqrt{\frac{a}{\rho}} \to \infty \, (\rho \to 0)$$

$$\boxed{K_t \to \infty}$$???

Stress Analysis of Members with Notches

Stress Concentration Factor, Kt

For An Elliptical Hole $K_t \rightarrow \infty$ Meaningless



A Different Approach is needed to analyze the behavior of structures containing cracks or sharp imperfections

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3.History of Fracture Mechanics

1921 Griffith

Griffith's Formula

1948 Irwin

1957 Irwin

Stress Intensity Factor, K

…..

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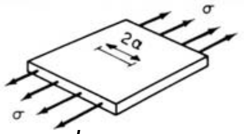
Griffith Theory

Consider an plate contains a through-thickness crack of length 2a and that is subjected to uniform tensile stress σ The total potential energy of the system, U is written as



$$U = U_o - U_a + U_\gamma$$

U_o : *elastic energy of the unclacked plate*

$$U_a = \frac{\pi \sigma^2 a^2}{E} : \textit{decrease in elastic energy caused by the crack}$$

$U_\gamma : 2(2a\gamma_e)$: *elasticsurface energy by the formation of the crack surface*

$$\frac{\partial U}{\partial a} = 0 \longrightarrow$$

$$\sigma\sqrt{a} = \boxed{\left(\frac{2\gamma_e E}{\pi}\right)^{1/2}}$$

const.

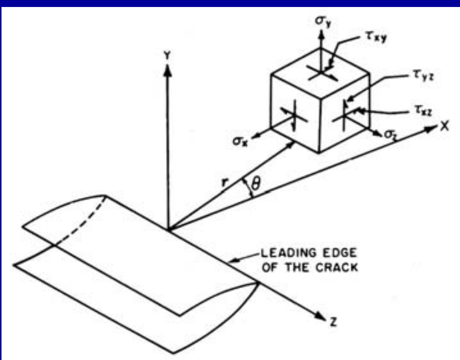
crack extension is governed by the crack length and the material property

4.Stress Analysis of Members with Notches

Stress Distribution along X-axis near the notch root

$$\frac{(\sigma_y)_{y=0}}{\sigma} = \frac{(\sigma_x)_{y=0}}{\sigma} = \sqrt{\frac{a}{2r+\rho}}$$

$$\rho \to 0$$



$$\frac{(\sigma_y)_{y=0}}{\sigma} = \sqrt{\frac{a}{2r+\rho}}\left(1 + \frac{\rho}{2r+\rho}\right) + \left(\frac{\rho}{2r+\rho}\right)$$

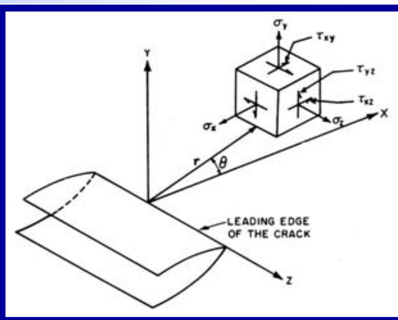
$$0 \le r << a, \ \rho << a$$

$$\frac{(\sigma_x)_{y=0}}{\sigma} = \sqrt{\frac{a}{2r+\rho}}\left(1 - \frac{\rho}{2r+\rho}\right)$$

Stress Analysis of Members with Cracks

$$\frac{(\sigma_y)_{y=0}}{\sigma} = \frac{(\sigma_x)_{y=0}}{\sigma} = \sqrt{\frac{a}{2r+\rho}}$$

$$\rho \to 0$$

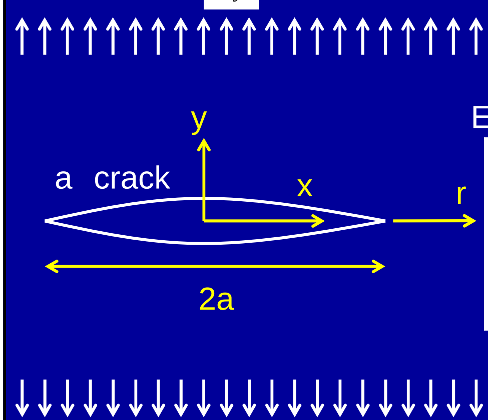


Stress near a crack tip

1. Singularity about $\dfrac{1}{\sqrt{r}}$
2. Intensity of Stress Singularity is Proportional to
   - far field stress σ_∞
   - square root of crack length a

Stress Analysis of Members with Cracks

σ_y^∞



σ_y^∞

Exact solution of stress near crack

$$\frac{(\sigma_y)_{y=0}}{\sigma} = \frac{|x|}{\sqrt{x^2-a^2}} = \frac{a+r}{\sqrt{r(2a+r)}}$$

$$\frac{(\sigma_x)_{y=0}}{\sigma} = \frac{|x|}{\sqrt{x^2-a^2}} - 1 = \frac{a+r}{\sqrt{r(2a+r)}} - 1$$

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Stress Analysis of Members with Cracks

$$\frac{(\sigma_y)_{y=0}}{\sigma} = \frac{|x|}{\sqrt{x^2-a^2}} = \frac{a+r}{\sqrt{r(2a+r)}}$$

$$\frac{(\sigma_x)_{y=0}}{\sigma} = \frac{|x|}{\sqrt{x^2-a^2}} - 1 = \frac{a+r}{\sqrt{r(2a+r)}} - 1$$

r/a<1

Series Expansion

$$\frac{(\sigma_y)_{y=0}}{\sigma} = \sqrt{\frac{a}{2r}} + \frac{3}{4}\sqrt{\frac{r}{2a}} - \frac{5}{32}\left(\sqrt{\frac{r}{2a}}\right)^3 + \cdots$$

$$\frac{(\sigma_x)_{y=0}}{\sigma} = \sqrt{\frac{a}{2r}} - 1 + \frac{3}{4}\sqrt{\frac{r}{2a}} - \frac{5}{32}\left(\sqrt{\frac{r}{2a}}\right)^3 + \cdots$$

$$\frac{(\sigma_y)_{y=0}}{\sigma} = \sqrt{\frac{a}{2r}} = \frac{\sigma\sqrt{\pi a}}{\sqrt{2\pi r}} = \frac{K}{\sqrt{2\pi r}}$$

$$\frac{(\sigma_x)_{y=0}}{\sigma} = \sqrt{\frac{a}{2r}} - 1$$

$$K = \sigma\sqrt{\pi a}$$

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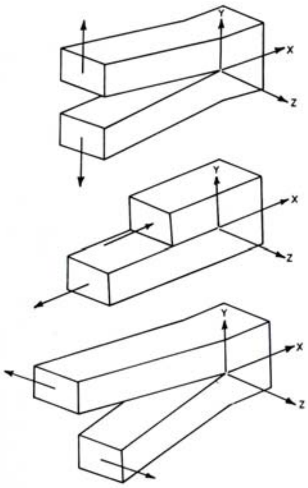
5.Stress Analysis for Cracks in Elastic Solids

Three Types of Relative Movements of Two Crack Surfaces



MODE I : Opening Mode

MODE II : Sliding/Shear Mode

MODE III : Tearing Mode

Basic Types of Stress Fields near Crack Tips

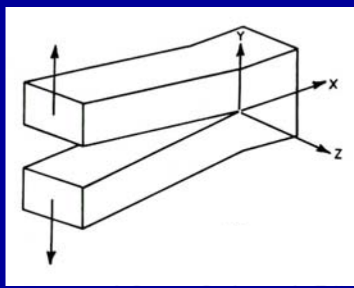
Important Basic Mode I

Most engineering situations corresponding to Mode I

$$\sigma_x = \frac{K_I}{(2\pi r)^{\frac{1}{2}}} \cos\frac{\theta}{2}\left[1 - \sin\frac{\theta}{2}\cdot\sin\frac{3\theta}{2}\right]$$

$$\sigma_y = \frac{K_I}{(2\pi r)^{\frac{1}{2}}} \cos\frac{\theta}{2}\left[1 + \sin\frac{\theta}{2}\cdot\sin\frac{3\theta}{2}\right]$$

$$\tau_{xy} = \frac{K_I}{(2\pi r)^{\frac{1}{2}}} \sin\frac{\theta}{2}\cdot\cos\frac{\theta}{2}\cdot\cos\frac{3\theta}{2}$$



$$u = \frac{K_I}{G}\left[\frac{r}{2\pi}\right]^{\frac{1}{2}} \cos\frac{\theta}{2}\left[1 - 2\nu + \sin^2\frac{\theta}{2}\right]$$

$$v = \frac{K_I}{G}\left[\frac{r}{2\pi}\right]^{\frac{1}{2}} \sin\frac{\theta}{2}\left[1 - 2\nu - \cos^2\frac{\theta}{2}\right]$$

$$w = 0$$

6. Stress Intensity Factor

The Applied Stress
The Crack Shape and Size
The Structural Configuration

⬇ Affect

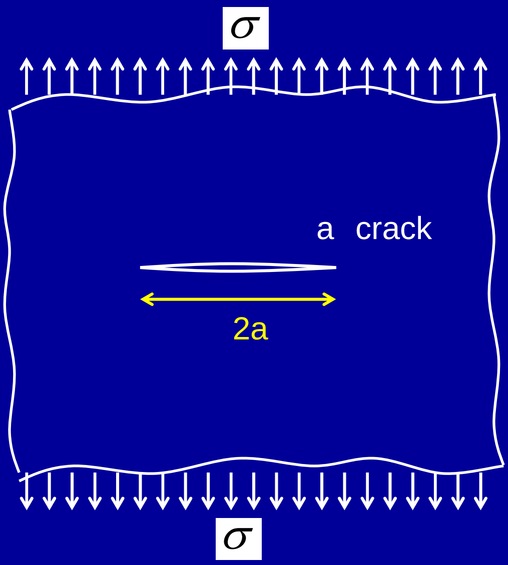
The Value of The Stress Intensity Factor, K

$$K = \sigma\sqrt{\pi a}\cdot F$$

F : Correction factor

Local Stress Field ⟷ Global Stress Field

Stress Intensity Factor Equations (1)



A Through Thickness Crack
In an Infinite Plate subject
to Uniform Tensile Stress

$$K = \sigma\sqrt{\pi a}$$

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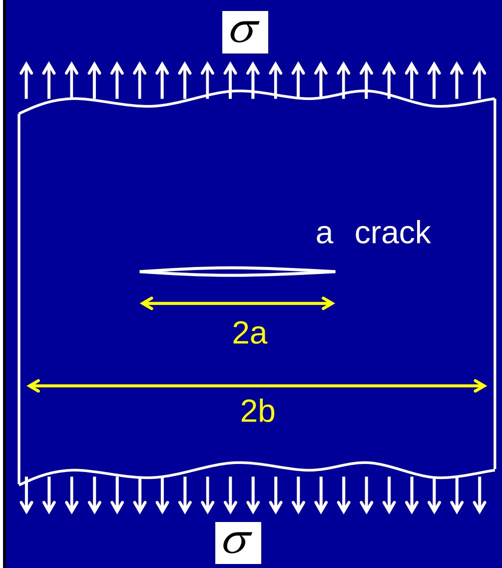
Stress Intensity Factor Equations (2)



A Through Thickness Crack
In a Plate with Finite Width
Subject to
Uniform Tensile Stress

$$K = \sigma\sqrt{\pi a}\left(\frac{2b}{\pi a}\tan\frac{\pi a}{2b}\right)^{\frac{1}{2}}$$

$$= \sigma\sqrt{\pi a}\sqrt{\sec\left(\frac{\pi a}{2b}\right)}$$

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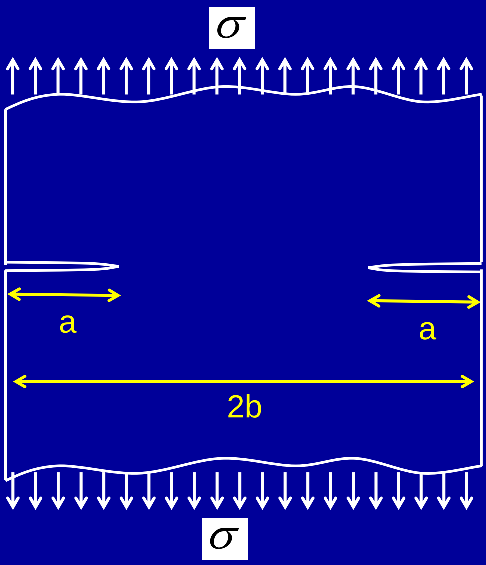
Stress Intensity Factor Equations (3)



Double-Edge Cracks
In a plate with finite width

$$K = \sigma\sqrt{\pi a} \cdot 1.12$$

original form

$$K = \sigma\sqrt{\pi a} \cdot F(\alpha), \alpha = \frac{a}{b}$$

$$F(\alpha) \cong \left(1 + 0.122\cos^2\frac{\pi\alpha}{2}\right)\sqrt{\frac{2}{\pi\alpha}\tan\frac{\pi\alpha}{2}}$$

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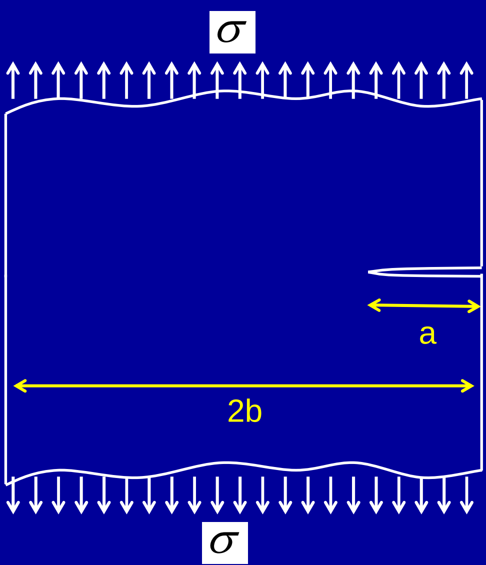
Stress Intensity Factor Equations (4)



Single-Edge Crack
In a plate with finite width

$$K = 1.12 \cdot \sigma\sqrt{\pi a} \cdot f\left(\frac{a}{b}\right)$$

a/b	f
0.1	1.03
0.2	1.07
0.3	1.15
0.5	1.35
0.7	1.69
0.9	2.20

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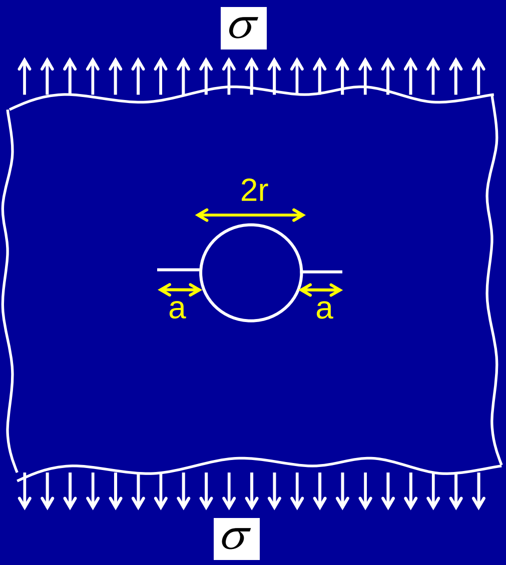
Stress Intensity Factor Equations (5)



Cracks growing from a round hole

$$K = \sigma\sqrt{\pi a}\cdot f\left(\frac{a}{r}\right)$$

$$a \to 0 \quad f\left(\frac{a}{r}\right) \to 3$$

For short cracks

$$K = K_t \sigma \sqrt{\pi a}$$

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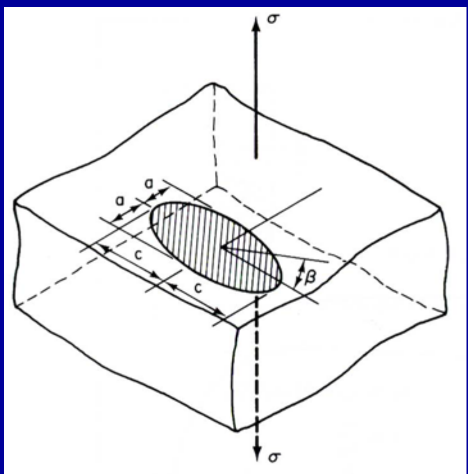
Stress Intensity Factor Equations (6)



An Embedded elliptical crack or a circular crack In an Infinite Plate

$$K = \frac{\sigma\sqrt{\pi a}}{\Phi_0}\left(\sin^2\beta + \frac{a^2}{c^2}\cos^2\beta\right)^{\frac{1}{4}}$$

$$\Phi_0 = \int_0^{\frac{\pi}{2}}\left[1-\left(\frac{c^2-a^2}{c^2}\right)\sin^2\theta\right]^{\frac{1}{2}} d\theta$$

$$K = \sigma\sqrt{\frac{\pi a}{Q}} \qquad for \quad \beta = \frac{\pi}{2}$$

$$Q = \Phi_0^2$$

$$K = 0.65\sigma\sqrt{\pi a} = 1.15\sigma\sqrt{a}$$

$$for \quad \beta = \frac{\pi}{2},\ a = c \quad (a\ circle)$$

$$K = \frac{2}{\sqrt{\pi}}\sigma\sqrt{a} = 1.13\sigma\sqrt{a}$$

Exact expression for circular crack

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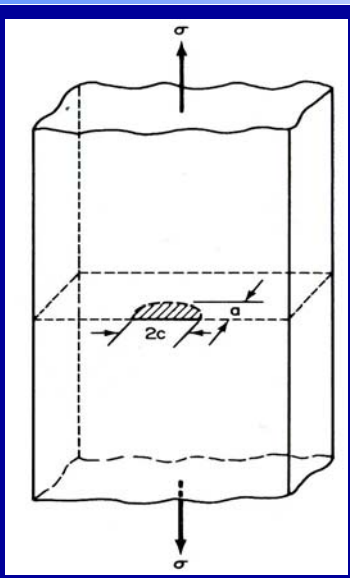
Stress Intensity Factor Equations (6)



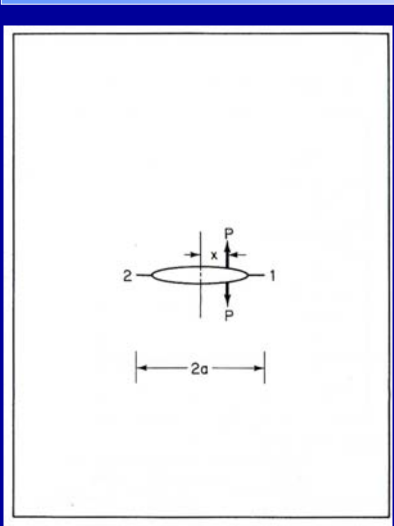
A Surface crack
or a circular crack
In an Infinite Plate

$$K = 1.12\sigma\sqrt{\pi\frac{a}{Q}}\cdot M_k$$

$$M_k = 1.0 + 1.2\left(\frac{a}{t} - 0.5\right)$$

t/a>0.5

Stress Intensity Factor Equations (7)



Cracks with wedge forces
and internal pressure

Eccentric line forces, P,
per unit thickness

$$K_{@1} = \frac{P}{\sqrt{\pi a}}\left(\frac{a+x}{a-x}\right)^{\frac{1}{2}}$$

$$K_{@2} = \frac{P}{\sqrt{\pi a}}\left(\frac{a-x}{a+x}\right)^{\frac{1}{2}}$$

$$K_{@1} = K_{@2} = \frac{P}{\sqrt{\pi a}} \quad at\ x = 0$$

$K = p\sqrt{\pi a}$: internal pressure

Engineering Calculation of Stress Intensity Factor

Pedro Albrecht/ K. Yamada, ASCE, STR, Feb.1977

$$K = F(a)\sigma\sqrt{\pi a}$$

$$F(a) = F_e \cdot F_s \cdot F_w \cdot F_g$$

Fe: The Shape of Crack Front, which is often assumed as an elliptical crack, correction

Fs: Effects of Free Surface, Front Free Surface Correction

Fw: Finite Width, The Back Surface Correction

Fg: Non-uniform Opening Stresses, Stress Gradient Correction

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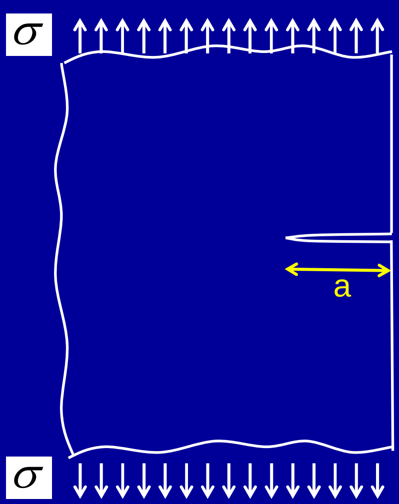
2 Dimensional Crack Problems(1)



The Edge Crack in a semi-infinite plate

$$K = F(a)\sigma\sqrt{\pi a}$$

$$F(a) = F_s = 1.12$$

Front Free Surface Correction

$$K = 1.12\sigma\sqrt{\pi a}$$

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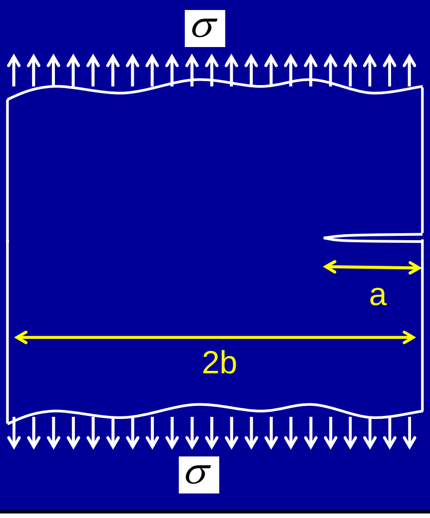
2 Dimensional Crack Problems(2)

Single-Edge Crack
In a plate with finite width



$$K = F(a)\sigma\sqrt{\pi a}$$

$$F(a) = F_s \cdot F_w$$

$$K = \underbrace{\boxed{1.12}}_{F_s}\,\sigma\sqrt{\pi a}\cdot \underbrace{\boxed{f\left(\frac{a}{b}\right)}}_{F_w}$$

F_s Front Free Surface Correction

F_w Finite Width

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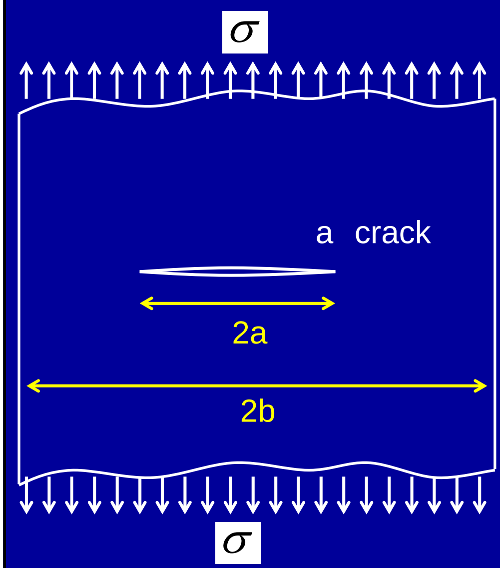
2 Dimensional Crack Problems (3)



A Through Thickness Crack
In a Plate with Finite Width
Subject to
Uniform Tensile Stress

$$K = \sigma\sqrt{\pi a}\boxed{\left(\frac{2b}{\pi a}\tan\frac{\pi a}{2b}\right)^{\frac{1}{2}}}$$

$$= \sigma\sqrt{\pi a}\boxed{\sqrt{\sec\left(\frac{\pi a}{2b}\right)}}$$

Finite Width $F(a) = F_w$

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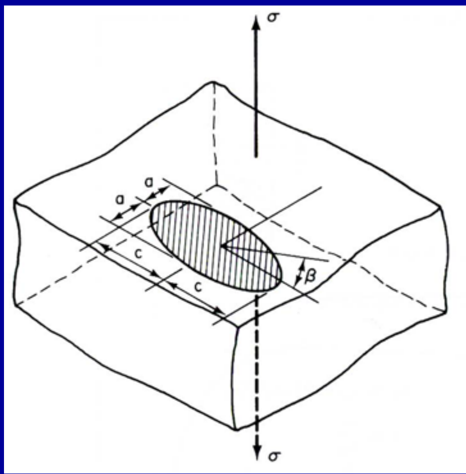
3 Dimensional Crack Problems (1)



An Embedded elliptical crack or a circular crack
In an Infinite Plate

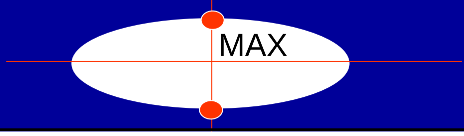
$$K = \frac{1}{\Phi_0}\left(\sin^2\beta + \frac{a^2}{c^2}\cos^2\beta\right)^{\frac{1}{4}} \cdot \sigma\sqrt{\pi a}$$

$$\Phi_0 = \int_0^{\frac{\pi}{2}} \left[1 - \left(\frac{c^2 - a^2}{c^2}\right)\sin^2\theta\right]^{\frac{1}{2}} d\theta$$

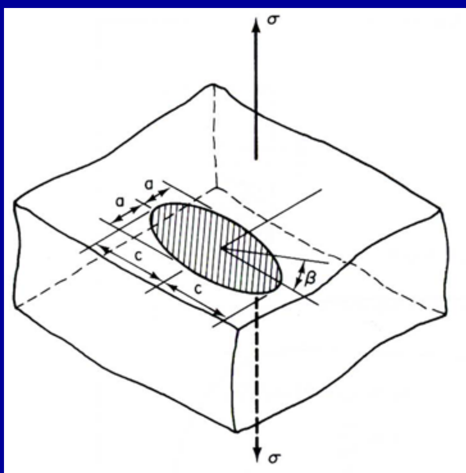
$$K = \boxed{\frac{1}{\Phi_0}}\sigma\sqrt{\pi a} \quad for \quad \beta = \frac{\pi}{2}$$

F_e

$$F(a) = F_e = \frac{1}{\Phi_0}$$



3 Dimensional Crack Problems (1)



An Embedded elliptical crack or a circular crack
In an Infinite Plate

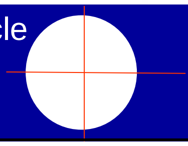
$$K = \frac{1}{\Phi_0}\left(\sin^2\beta + \frac{a^2}{c^2}\cos^2\beta\right)^{\frac{1}{4}} \cdot \sigma\sqrt{\pi a}$$

$$\Phi_0 = \int_0^{\frac{\pi}{2}} \left[1 - \left(\frac{c^2 - a^2}{c^2}\right)\sin^2\theta\right]^{\frac{1}{2}} d\theta$$

$$K = \boxed{\frac{1}{\Phi_0}}\sigma\sqrt{\pi a} \quad for \quad \beta = \frac{\pi}{2}$$

F_e

Circle

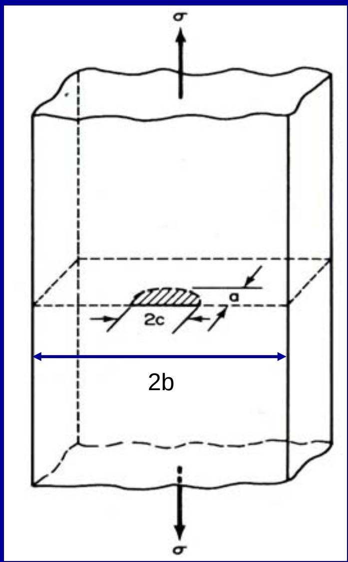


$$K = \frac{2}{\pi}\sigma\sqrt{\pi a}$$

$$F(a) = F_e = \frac{1}{\Phi_0} = \frac{2}{\pi}$$

$for \ a = c$

3 Dimensional Crack Problems (2)



A Surface crack
or a circular crack
In a Plate with Finite Width

$$K = \boxed{\alpha \cdot M_k} \cdot \boxed{\frac{1}{\Phi_0}} \cdot \boxed{F_g} \cdot \sigma\sqrt{\pi a} \cdot \boxed{\sqrt{\frac{2b}{\pi a}\tan\frac{\pi a}{2b}}}$$

F_s F_e F_w

$$M_k = 1.0 + 1.2\left(\frac{a}{t} - 0.5\right)$$

Stress Gradient Correction
Correction for Stress Concentration

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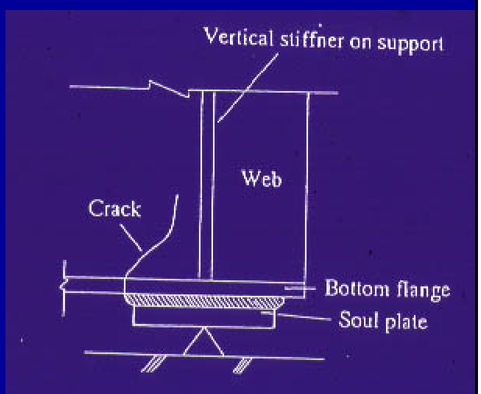
Geometry Correction Factor F_g

Cracks always occur at geometrical discontinuities as cover plate ends …..



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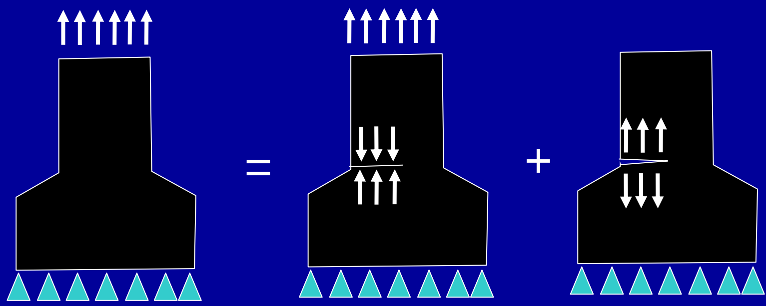
Calculation of F_g

Superimpose



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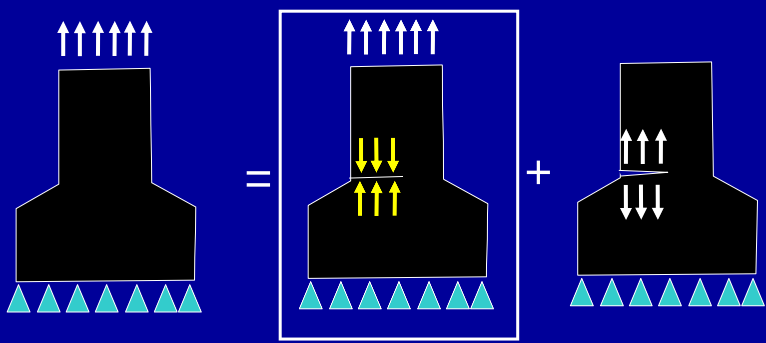
Calculation of F_g

Superimpose



Step 1

Compute the actual stress
Along the line where the crack
would be inserted FEM
By any suitable methods.

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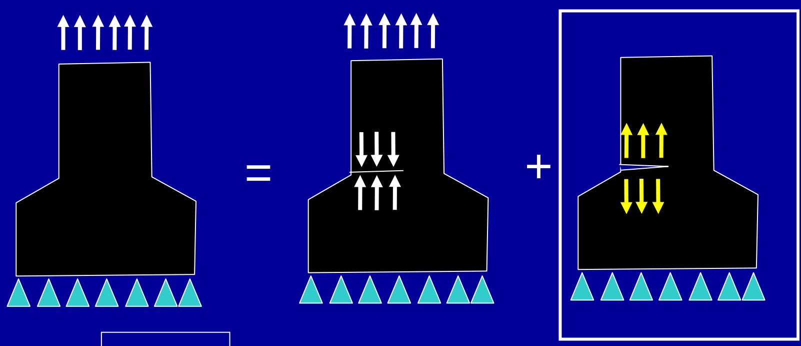
Calculation of F_g

Superimpose



Step 2

Insert a crack of given length
Along the same line and apply
the stress determined in Step1

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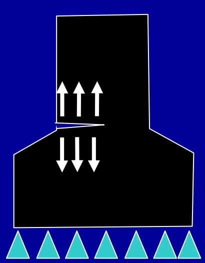
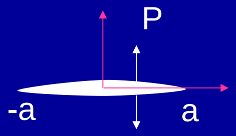
Calculation of F_g





$$K_i = \frac{P_i + P_i'}{2\sqrt{\pi a}}\sqrt{\frac{a+x}{a-x}}$$

$$K = \int_{-a}^{a}\left(\frac{\sigma + \sigma'}{2\sqrt{\pi a}}\sqrt{\frac{a+x}{a-x}}\right)dx$$

Step 3

Compute K by integrating Ki over the
length of the crack with the stress
determined in Step 1 applied

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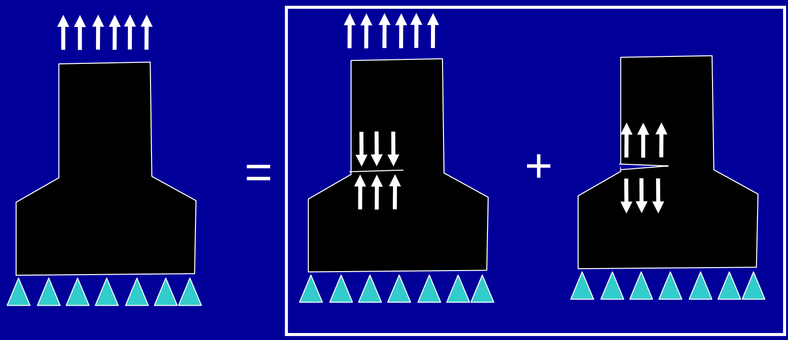
Calculation of F_g

Superimpose



Step 4

Repeat steps 2 and 3
for any desired crack size

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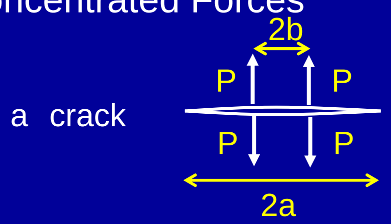
Calculation of F_g

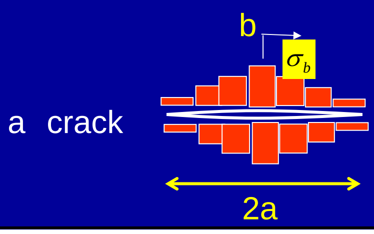
Calculation of K in Step 3

Concentrated Forces



$$K = \frac{2P}{\sqrt{\pi a}} \frac{a}{\sqrt{a^2 - b^2}}$$

Distributed Forces



$$K = \sqrt{\pi a}\, \frac{2}{\pi} \int_0^a \frac{\sigma_b}{\sqrt{a^2 - b^2}} db$$

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Calculation of F_g

Stress Distribution in Step 1

Closed form expressions defining the stress distribution In the uncracked body are usually not available.

From FEM

$$K = \sqrt{\pi a}\,\frac{2}{\pi}\sum_{i=1}^{n}\sigma_{b_i}\int_{b_i}^{b_{i-1}}\frac{1}{\sqrt{a^2-b^2}}db$$

In which the discrete stress σ_{b_i} is applied over the element b_i and b_{i+1}

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Calculation of F_g

Stress Distribution in Step 1

After factoring out the mean stress

$$K = \sqrt{\pi a}\,\frac{2}{\pi}\sum_{i=1}^{n}\sigma_{b_i}\int_{b_i}^{b_{i-1}}\frac{1}{\sqrt{a^2-b^2}}db$$

$$K = \sigma\sqrt{\pi a}\,\frac{2}{\pi}\sum_{i=1}^{n}\frac{\sigma_{b_i}}{\sigma}\left(\arcsin\frac{b_{i-1}}{a} - \arcsin\frac{b_i}{a}\right)$$

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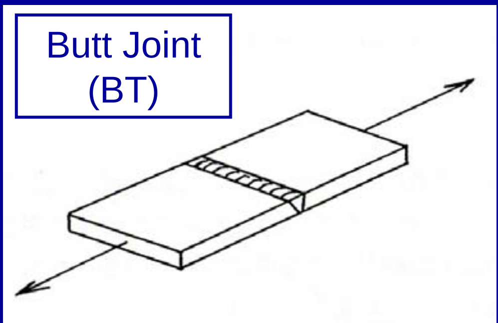
Examples of F_g



$$F_g = 1$$

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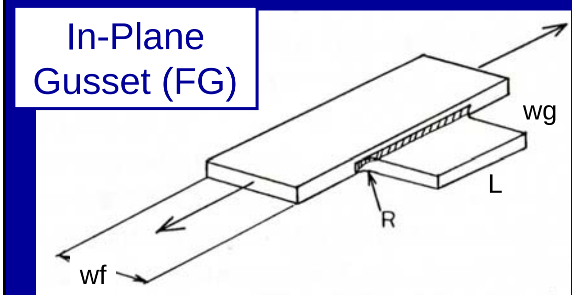
Examples of F_g



$$F_g = \frac{-1.115\log(\frac{R}{w_f}) + 0.537\log(\frac{L}{w_f}) + 0.1384\log(\frac{w_g}{w_f}) + 0.6801}{1 + \frac{1}{1.158} \cdot (\frac{a}{w_f})^{0.6051}}$$

By Zettlemoyer and Fisher

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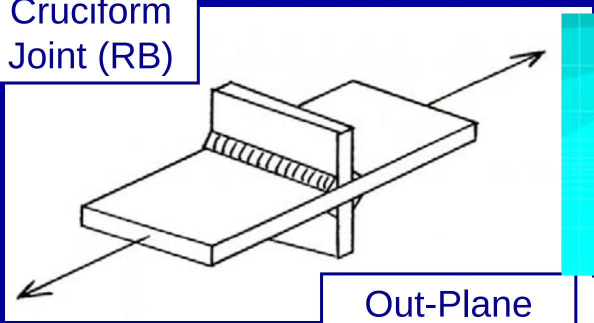
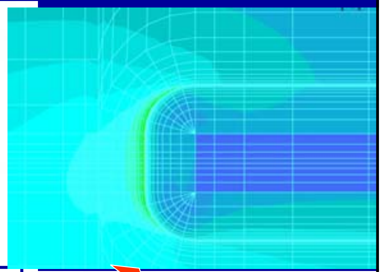
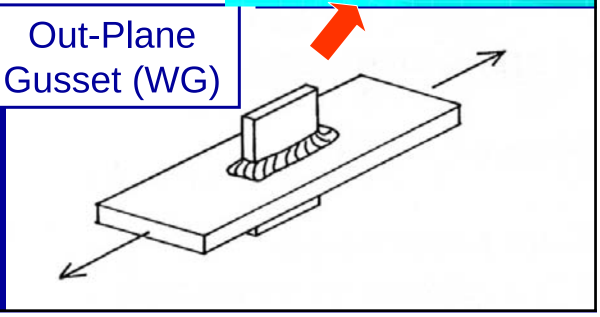
Examples of F_g

Cruciform Joint (RB)

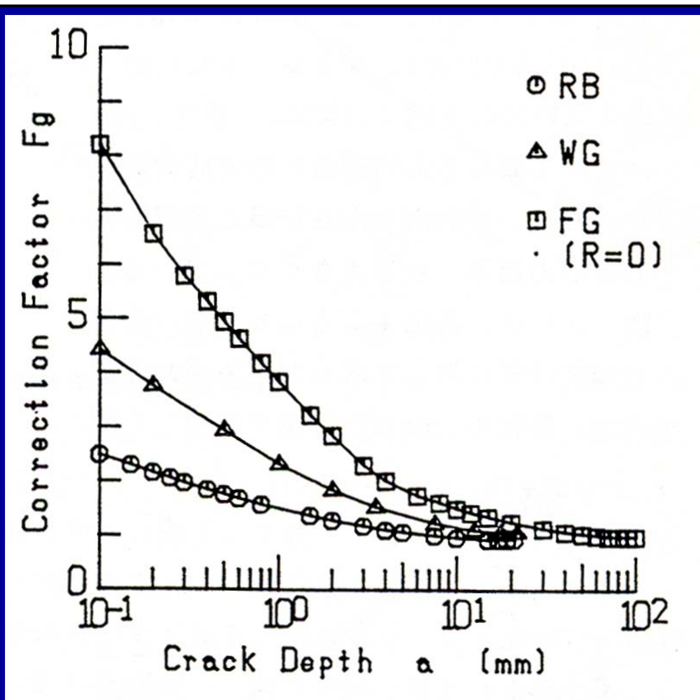




Out-Plane Gusset (WG)



Stress Distribution From FEM



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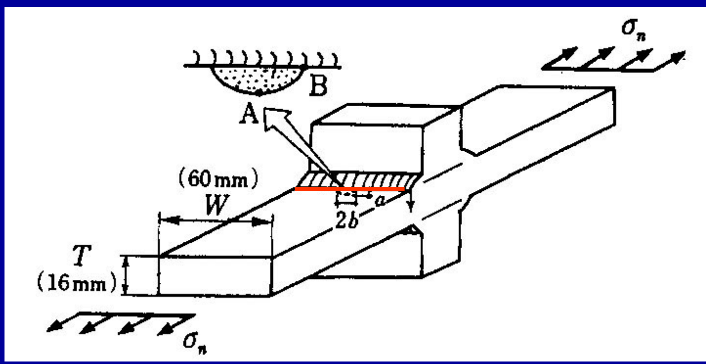
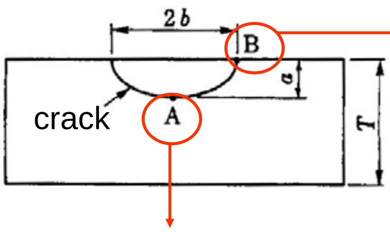
Examples of F_g

Cracks from Incomplete Penetration



Model of Cracks



$$\Delta K_B = F_{eB} \cdot F_{tB} \cdot F_{gB} \cdot \Delta\sigma \cdot \sqrt{\pi a}$$

$$F_{eB} = F_{eA} \Big/ \sqrt{a/b}$$

$$F_{tB} = (1 - 0.025k^2 + 0.06k^4)\sqrt{\sec(\pi k/2)}$$

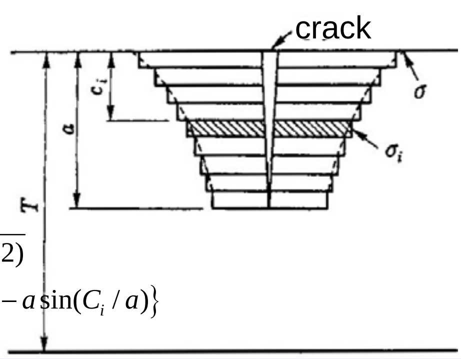
$$\Delta K_A = F_{eA} \cdot F_{sA} \cdot F_{tA} \cdot F_{gA} \cdot \Delta\sigma \cdot \sqrt{\pi a}$$

$$F_{eA} = 1 \Big/ \sqrt{1 + 1.464(a/b)^{1.65}}$$

$$F_{sA} = 1 + 0.12(1 - a/b)$$

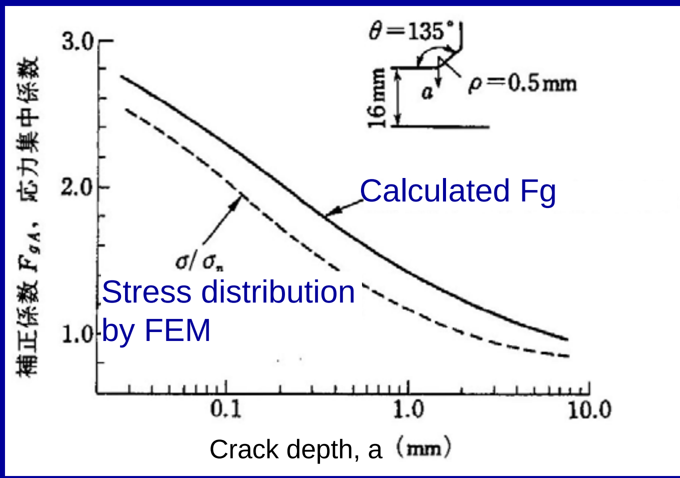
$$F_{tA} = (1 - 0.025\lambda^2 + 0.06\lambda^4)\sqrt{\sec(\pi\lambda/2)}$$

$$F_{gA} = (2/\pi)\sum(\sigma_i/\sigma_n)\{a\sin(C_{i+1}/a) - a\sin(C_i/a)\}$$

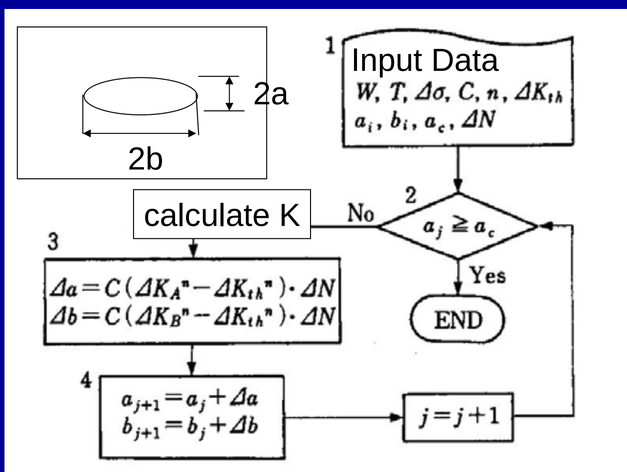


Calculation of Fg

Relationships of stress distribution and Fg

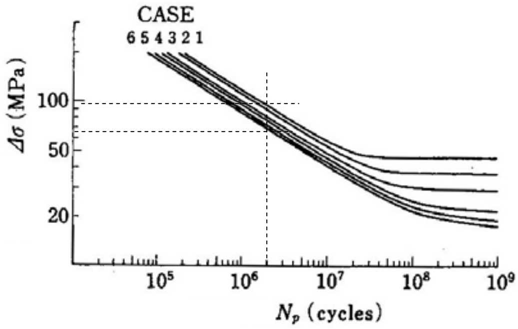


Calculation strategies



Results

Variation of initial crack width and height



Initial crack geometry

CASE	depth a (mm)	width $2b$ (mm)
1	0.1	0.4
2	0.2	0.8
3	0.5	2.0
4	1.0	4.0
5	1.5	6.0
6	2.0	8.0

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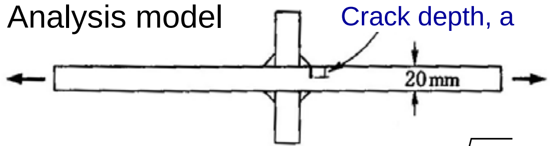
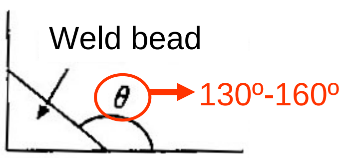
Effects of weld shape

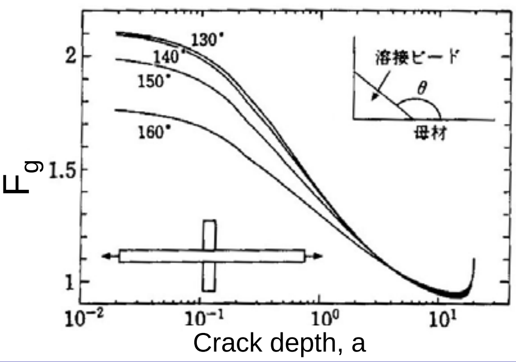
Analysis model



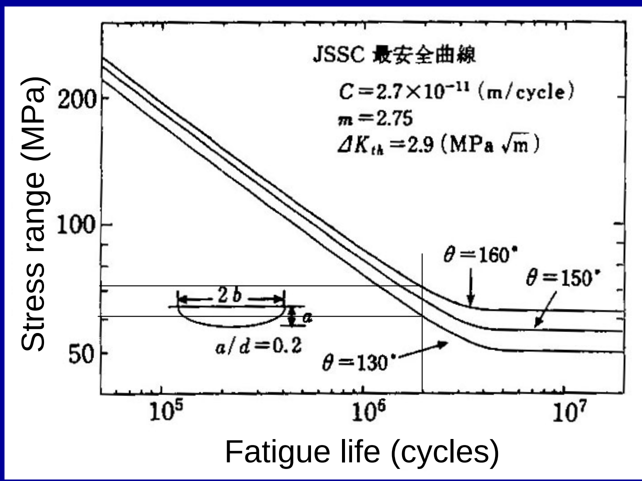
a_o = 0.1 mm
$2b_o$ = 1.0 mm

$$\Delta K_A = F_{eA} \cdot F_{sA} \cdot F_{tA} \cdot F_{gA} \cdot \Delta\sigma \cdot \sqrt{\pi a}$$

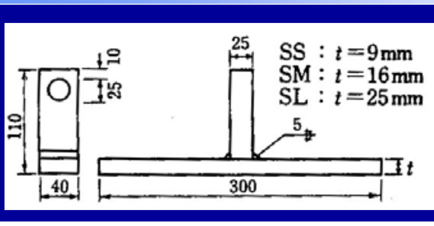




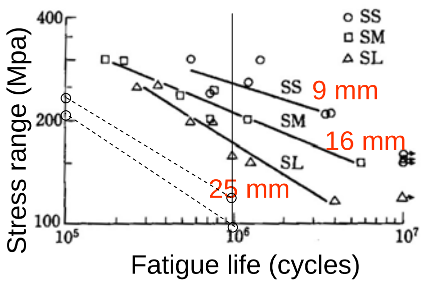
Effects of weld shape



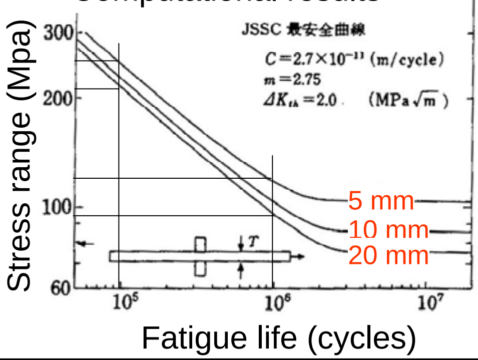
Effects of plate thickness



Experimental results



Computational results



Fracture Toughness

The Condition for Unstable Crack Growth

$$K = K_c$$

Fracture Toughness

The Critical Stress Intensity Factor for Unstable Crack Growth

Mode I

$$K_I = K_{Ic}$$

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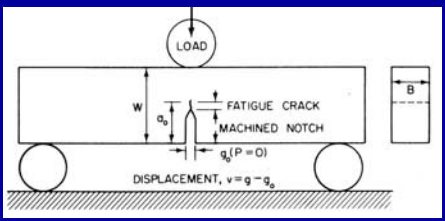
Test Methods to Evaluate K_{Ic}

ASTM E-399

A Bend Specimen



three point bend test

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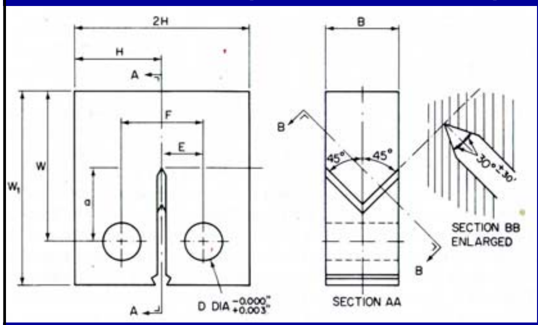
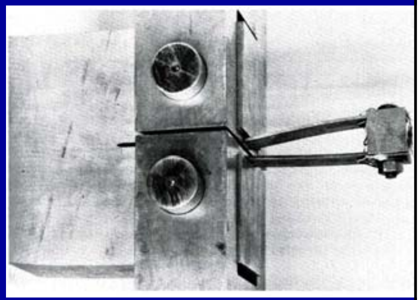
Test Methods to Evaluate K_{Ic}

ASTM E-399

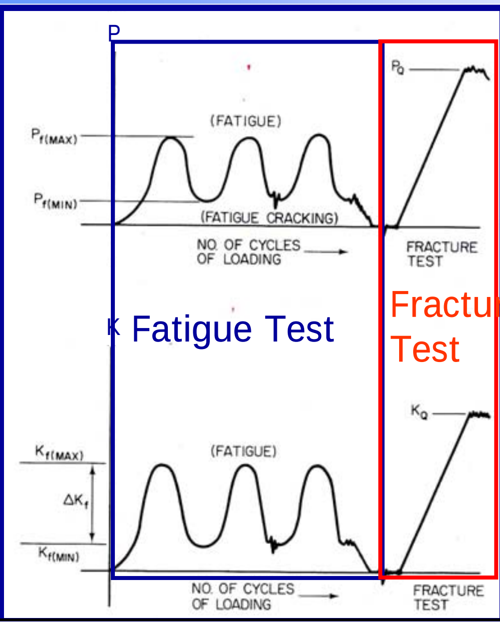
Compact Tension Specimen





Chevron notch : to keep the crack in plane and to ensure that it extended beyond the machined notch root (0.05W)

Test Methods to Evaluate K_{Ic}



The Testing Program

Fatigue Cracking

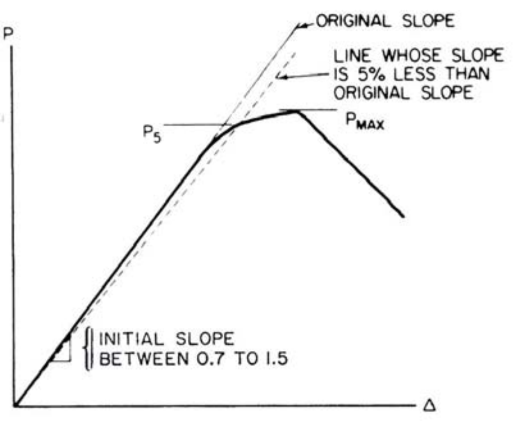
Small Scale Yielding Condition

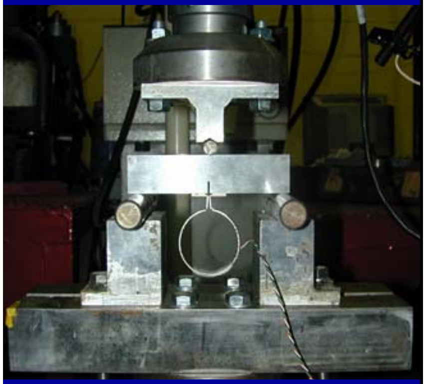
Fracture Test

Plane Strain Condition

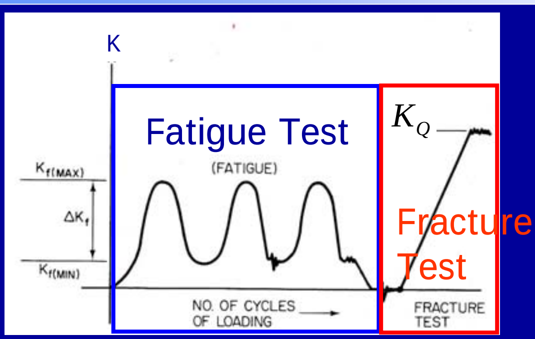
Test Methods to Evaluate K_{Ic}

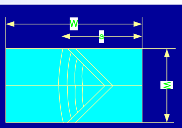
in Plane Fracture Toughness Testing





Test Methods to Evaluate K_{Ic}



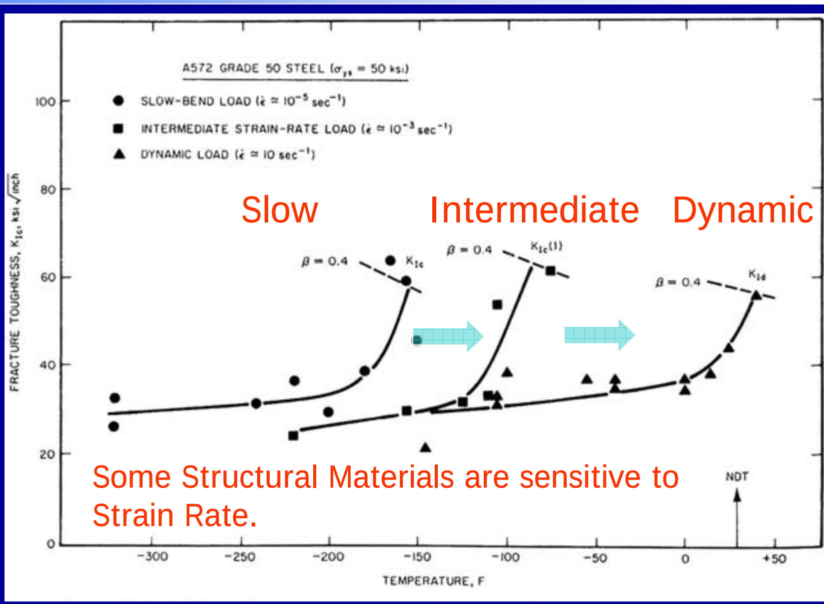


specimen minimum size requirement
a: crack length,
B: thickness
W : specimen depth

$$a \geq 2.5\left(\frac{K_Q}{\sigma_{Yield}}\right)^2, B \geq 2.5\left(\frac{K_Q}{\sigma_{Yield}}\right)^2, W \geq 5.0\left(\frac{K_Q}{\sigma_{Yield}}\right)^2$$

$$K_Q \Rightarrow K_{Ic}$$

Effects of Loading Rate on Fracture Toughness



Some Structural Materials are sensitive to Strain Rate.

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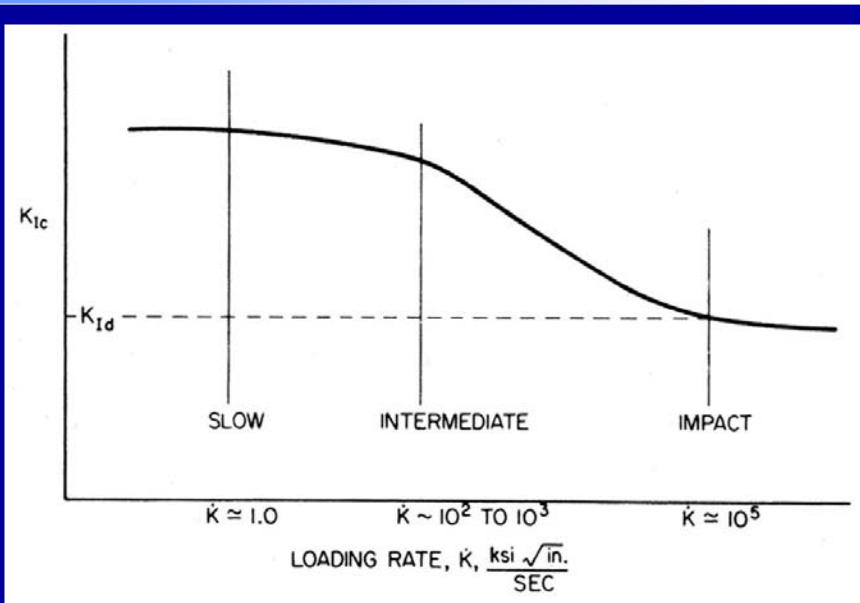
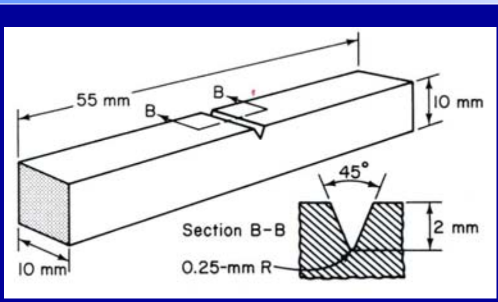
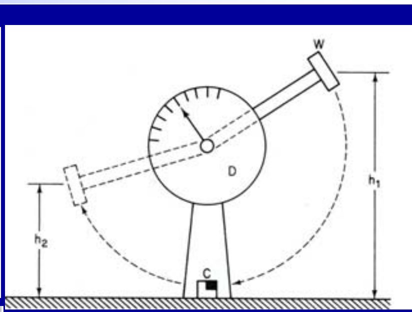
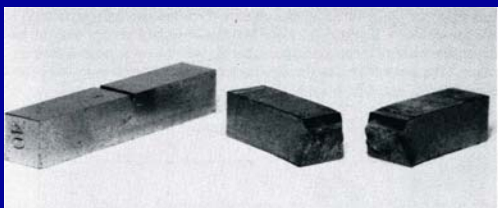
Effects of Loading Rate on Fracture Toughness



Charpy V-Notch (CVN) Impact Tests





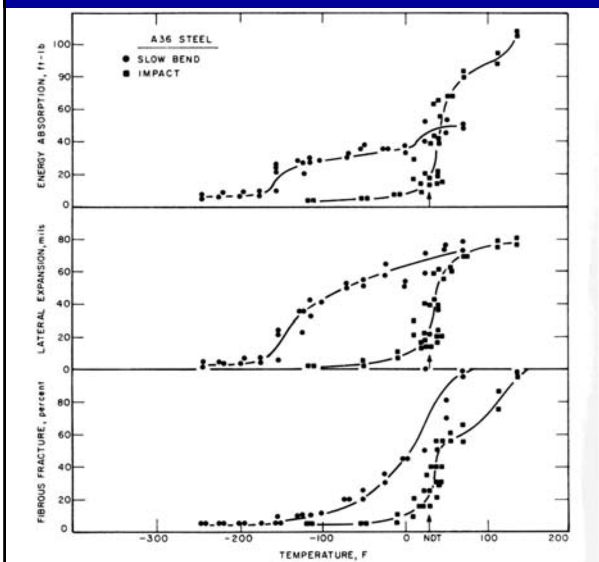


Dimension of a CVN specimen.
Specimen before and after tesing.

the energy absorbed by the specimen is related to the height differential h1-h2, is recorded on dial D.

The Traditional Evaluation Method of Fracture Toughness

Charpy Impact Tests



To Prevent
Brittle Fracture

Absorbed Energy: Ev

Transition Temperature: Ttr

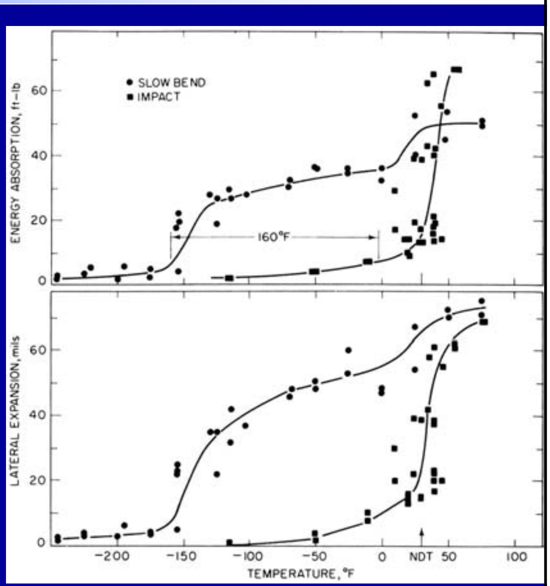
Absorbed Energy-Temperature

CVN Tests vs K_{Ic} Tests

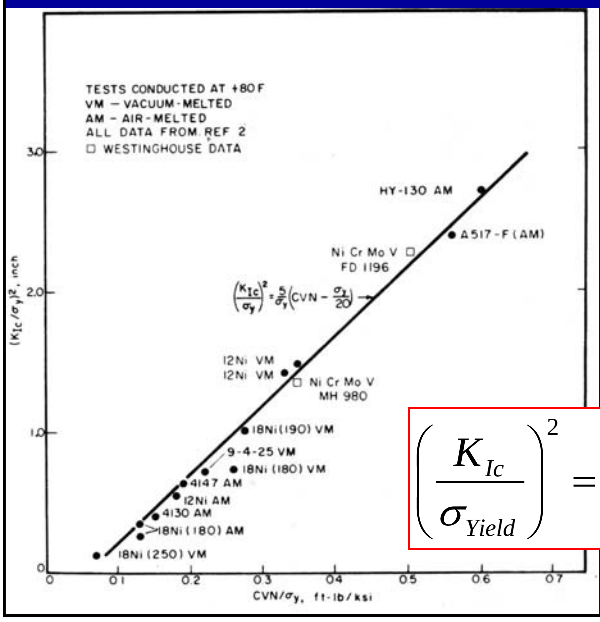
CVN Tests:
Dynamic Condition
Crack Initiation
+ Propagation

⇕

K_{Ic} Tests:
Slow Bending
Crack Initiation



K1c- CVN Upper Shelf Correlation



Proposed by
Barsom and Rolf

$$\left(\frac{K_{Ic}}{\sigma_{Yield}}\right)^2 = 5\left(\frac{CVN}{\sigma_{Yield}} - 0.05\right)$$