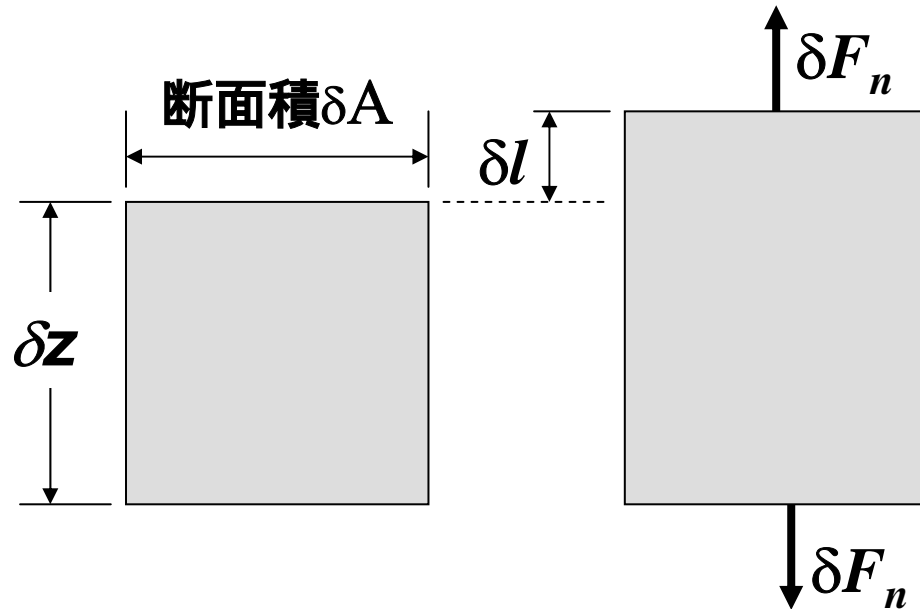


# 応力とひずみ (stress & strain)

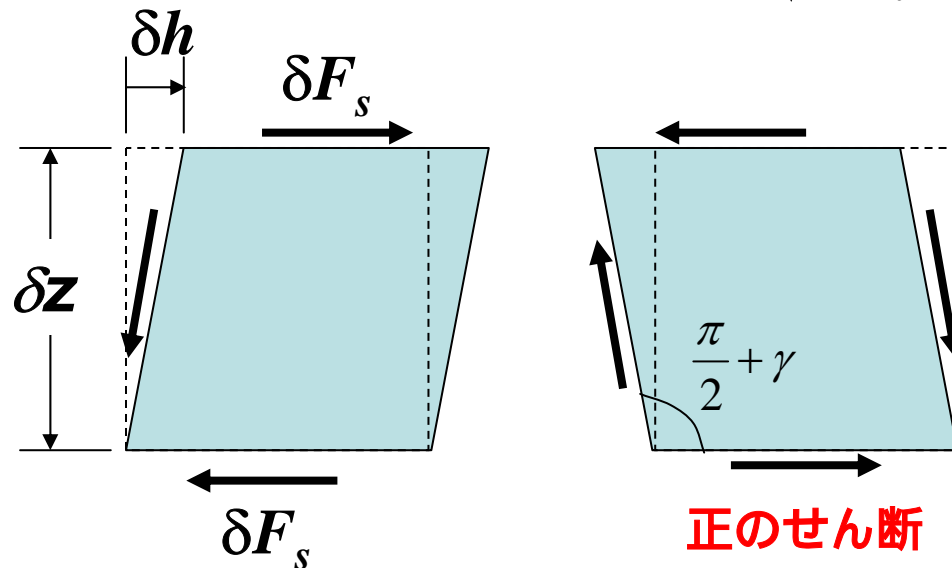


直応力:  $\delta\sigma = -\frac{\delta F_n}{\delta A}$   
(normal stress)

直ひずみ:  $\delta\varepsilon = -\frac{\delta l}{\delta z}$   
(normal strain)

## 土質力学の符号

- 直応力、ひずみ:  
圧縮を正
- せん断応力、ひずみ:  
反時計周りを正

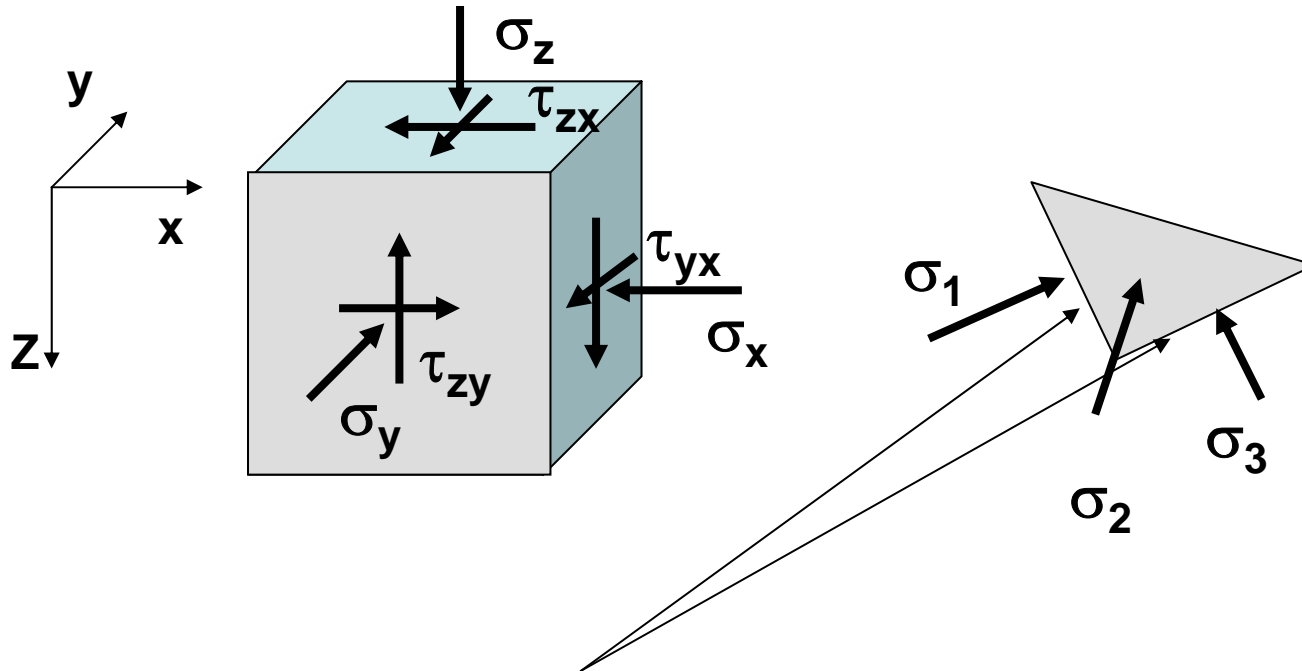


せん断応力:  $\delta\tau = -\frac{\delta F_s}{\delta A}$   
(shear stress)

せん断ひずみ:  $\delta\gamma = -\frac{\delta h}{\delta z}$   
(shear strain)

# 一般的な微小土要素の応力表示

応力: 方向によって変化する。

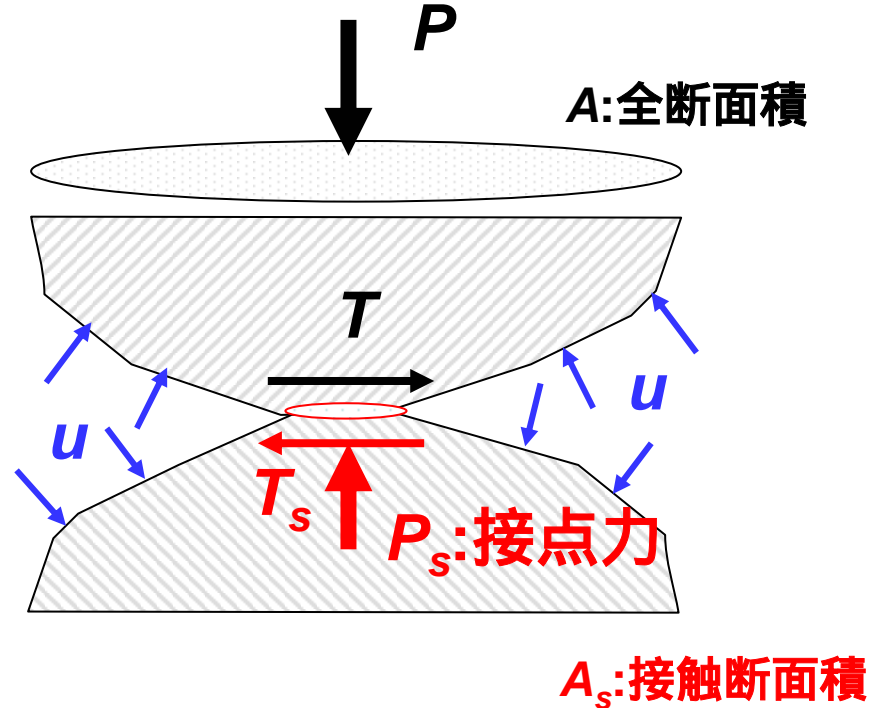


主応力面: せん断力がゼロの面 (互いに直交)  
(principal plane)

主応力面上の直応力 (principal stresses)

最大主応力 ( $\sigma_1$ ) > 中間主応力 ( $\sigma_2$ ) > 最小主応力 ( $\sigma_3$ )  
(major) (intermediate) (minor)

# 土要素内の力釣合い



全断面

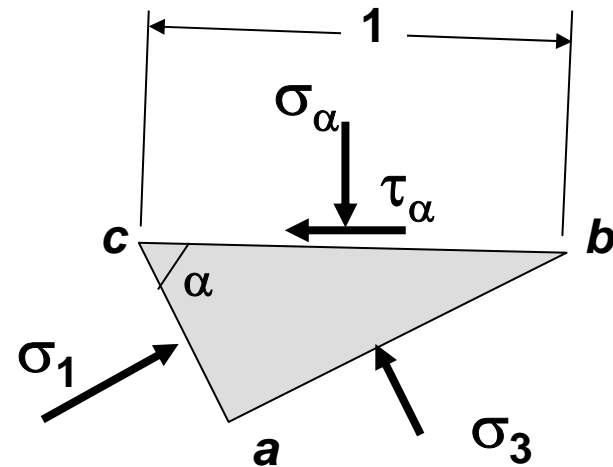
直応力:  $\sigma = \frac{P}{A}$ , せん断(応)力:  $\tau = \frac{T}{A}$

粒子積極面

直応力:  $\sigma_s = \frac{P_s}{A_s}$ , せん断(応)力:  $\tau_s = \frac{T_s}{A_s}$

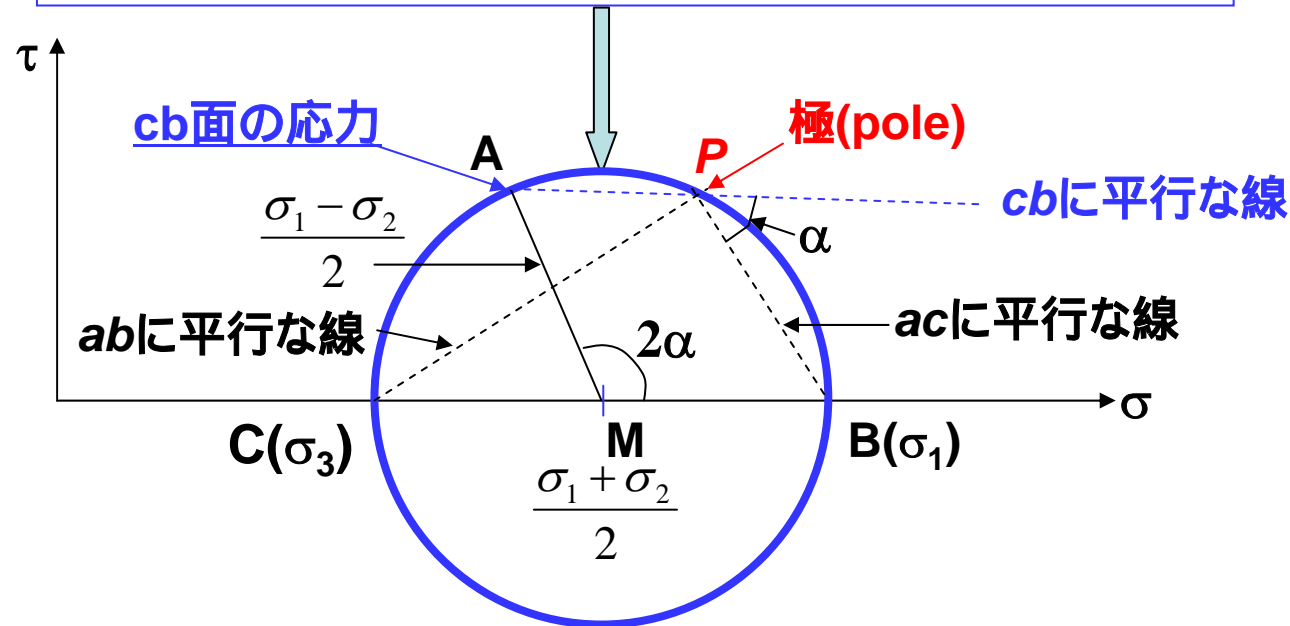
# モールの応力円(2次元) (Mohr's stress circle)

力の釣合い



$$\sigma_{\alpha} = \sigma_1 \cos^2 \alpha + \sigma_3 \sin^2 \alpha = \frac{\sigma_1 + \sigma_3}{2} + \frac{\sigma_1 - \sigma_3}{2} \cos 2\alpha$$

$$\tau_{\alpha} = (\sigma_1 - \sigma_3) \sin \alpha \cos \alpha = \frac{\sigma_1 - \sigma_3}{2} \sin 2\alpha$$



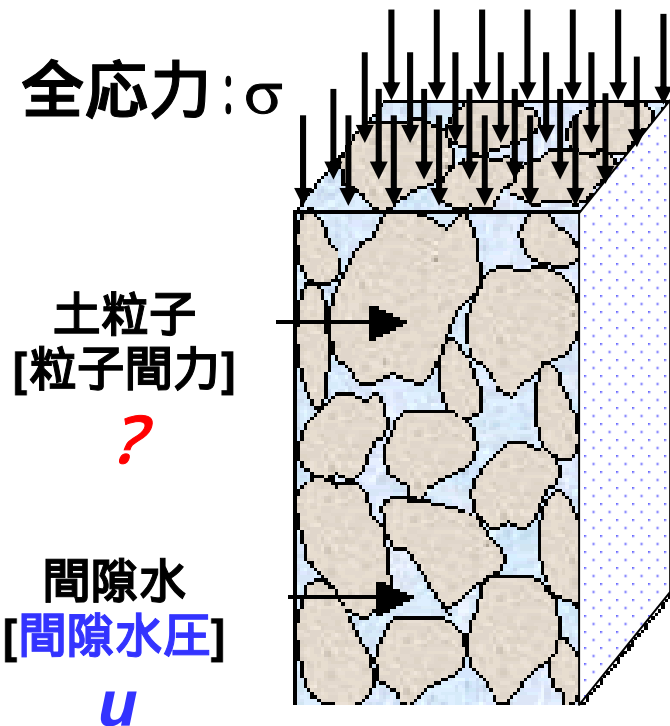
**極(pole):**

(傾き、応力成分) 既知の面があり、モールの応力円上のその点から面と平行な線を引き、円と交わった点。 => 極から任意の傾きの線を引きモール円と交わった点の応力は、その線と平行な面上の応力成分

# 地盤中の応力 (有効応力、全応力、間隙水圧)

## 土要素境界、内の応力

境界の直応力:  $\sigma$  => 全応力 (total stress)



Terzaghi (1923)

$$\sigma' = \sigma - u \quad (1)$$

有効応力  
(effective stress)

間隙水圧  
pore water pressure

飽和土

# 土要素内の力釣合い

## 面と垂直な方向の力の釣合い

Aで割る  
 $a = \frac{A_s}{A}$   $\longrightarrow$   $\downarrow$

$$P = P_s + (A - A_s)u$$
$$\sigma = a\sigma_s + (1-a)u$$
$$a = \frac{\sigma - u}{\sigma_s - u}$$

inter-granular stress  
(粒子間力 / 全断面)  $\sigma_g = \frac{P_s}{A}$

$$\sigma_g = \frac{P - (A - A_s)u}{A}$$
$$= \sigma - (1-a)u$$

$\downarrow$

$$\sigma_g = \sigma'$$

$a \sim 0$   
(接点面積0)

## 面と平行な方向の力の釣合い

水強度ゼロ  $\longrightarrow$   $T = T_s \rightarrow \tau = a\tau_s$

有効応力  $\leq$  粒子接点力

せん断応力: 全応力 = 有効応力

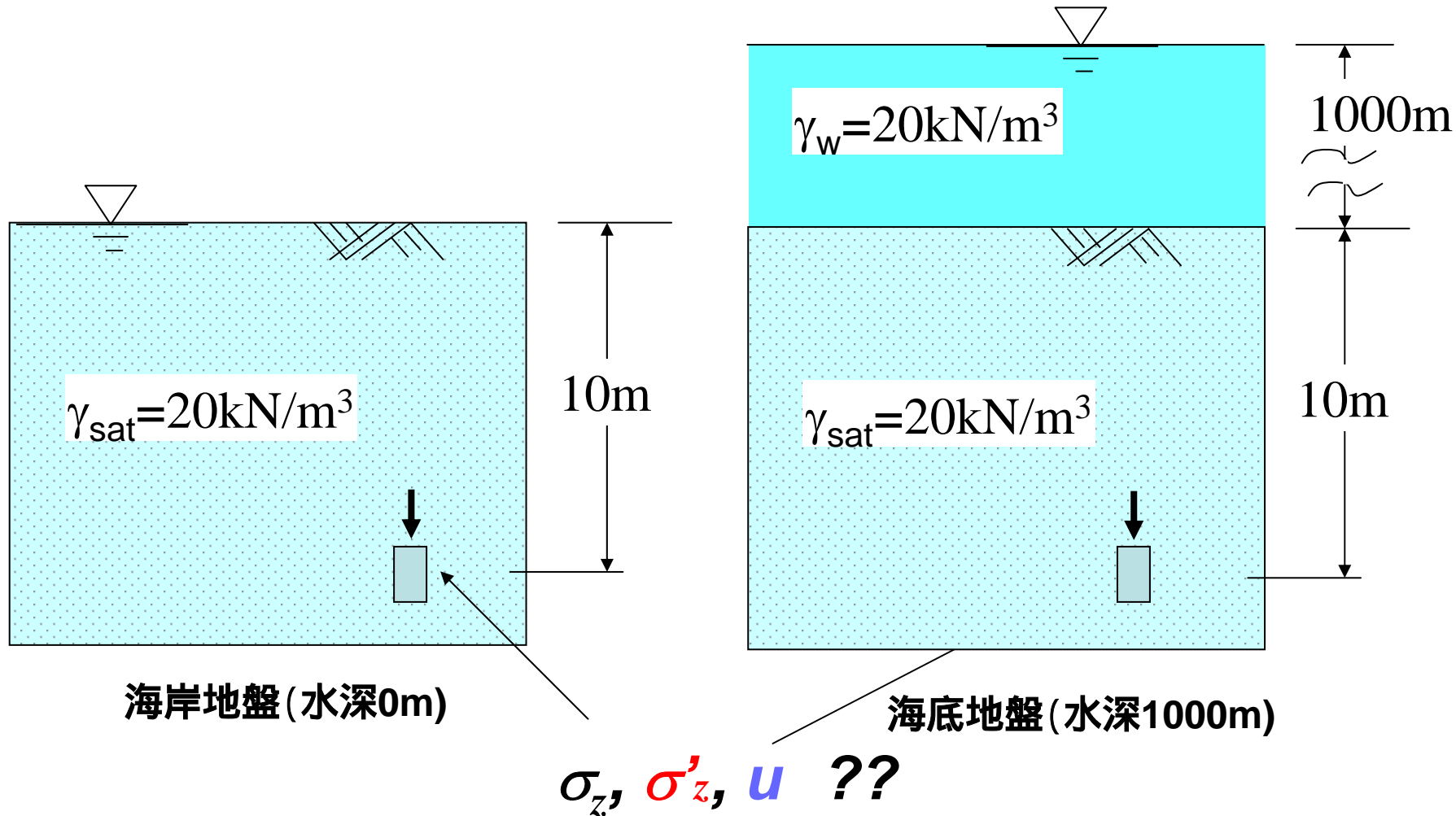
# 有効応力の原理 by K. Terzaghi (1937)

## (The principle of effective stress)

The stresses in any point of a section through a mass of soil can be computed from the total principal stress,  $\sigma_1, \sigma_2, \sigma_3$ , which act at this point. If the voids of the soil are filled with water under a stress  $u$ , the total stresses consist of two parts. One part  $u$  acts in the water and in the solid in every direction with equal intensity. It is the neutral stress (or pore pressure). The balance  $\sigma'_1 = \sigma_1 - u$ ,  $\sigma'_2 = \sigma_2 - u$  and  $\sigma'_3 = \sigma_3 - u$  represents an excess over the neutral stress  $u$  and it has its seat exclusively in the solid phase of the soil. This fraction of the total principal stress will be called the effective stress.

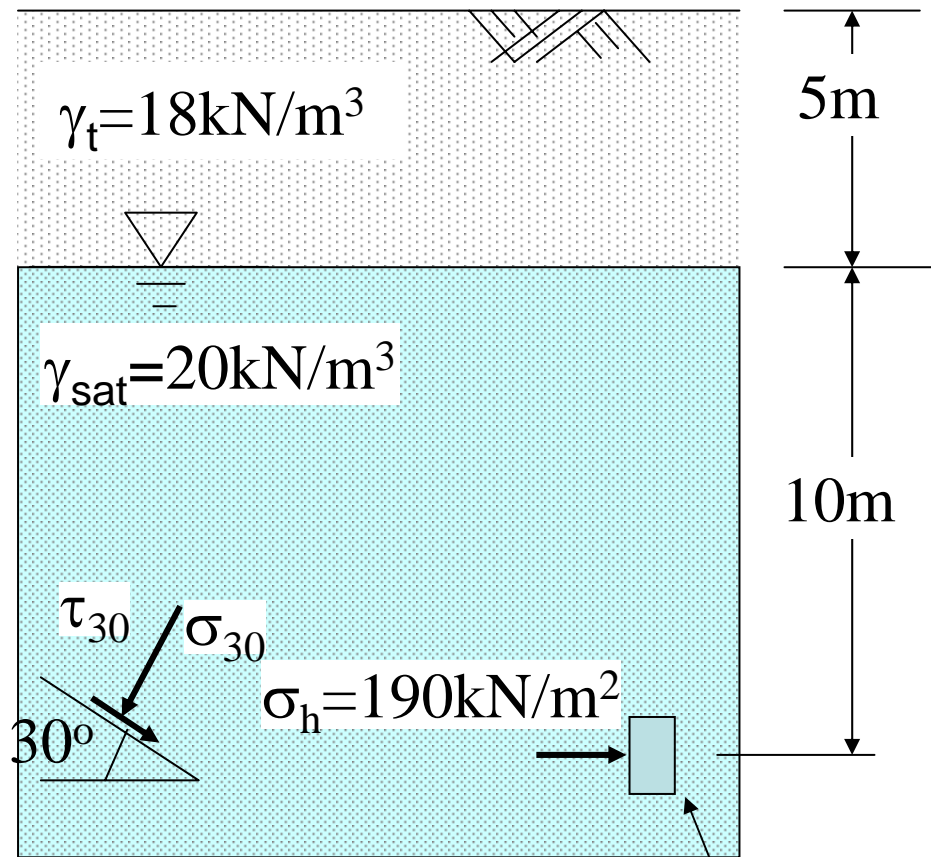
All measurable effects of a change of stress, such as compression, distortion and a change of shearing resistance, are due exclusively to changes of effective stress. The effective stress  $\sigma'$  is related to the total stress and pore pressure by  $\sigma' = \sigma - u$ . (宿題: この翻訳)

# 地盤中の応力



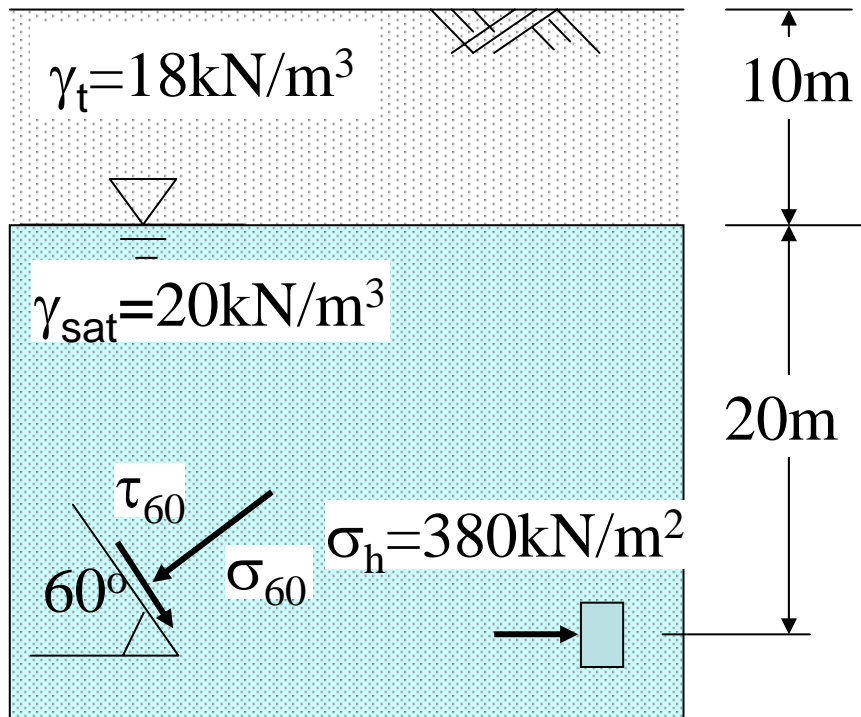


# 地盤中の応力



$\sigma_z, \sigma'_z, u$  ??  
モールの応力円、極

# 小テスト



$\sigma_z$ ,  $\sigma'_z$ ,  $u$  ??

全応力、有効応力のモール円、極の位置

# 本日のTechnical terms

応力: stress; ひずみ: strain

直応力: normal stress; 直ひずみ: normal strain

せん断応力: shear stress; せん断ひずみ: shear strain

全応力: total stress;

有効応力: effective stress;

間隙水圧: pore water pressure;

有効応力原理: The principle of effective stress;

主応力: principal stresses

最大主応力: major principal stress

中間主応力: intermediate principal stress

最小主応力: minor principal stress

モールの応力円: Mohr's stress circle

(モール円の)極: pole